I. CALL TO ORDER

II. ROLL CALL:
   Chair: Bob Cotterell
   Commissioners: Ken Hoffine, Stuart Liebowitz, Noel Groshong
                  John Seward, Vern Munion, Fred Dayton
                  Pat Lewandowski, Roger Whitcomb

III. APPROVAL OF MINUTES
   A. Special Meeting January 23, 2020

IV. DISCUSSION ITEMS
   A. Standby Generator Evaluation Study – Project No. 20WA03

AUDIENCE PARTICIPATION — At this time, anyone wishing to address the Commission concerning items of interest not included in the agenda may do so. The person addressing the Commission shall, when recognized, give his/her name for the record. All remarks shall be directed to the whole Commission. The Commission reserves the right to delay any action, if required, until such time when they are fully informed on the matter.

V. INFORMATIONAL

VI. BUSINESS FROM THE COMMISSION

VII. NEXT MEETING DATE: March 12, 2020

VIII. ADJOURNMENT

* * * AMERICANS WITH DISABILITIES ACT NOTICE * * *
Please contact the Office of the City Recorder, Roseburg City Hall, 900 SE Douglas Avenue, Roseburg, OR 97470-3397 (Phone 541-492-6700) at least 48 hours prior to the scheduled meeting time if you need an accommodation. TDD users please call Oregon Telecommunications Relay Service at 1-800-735-2900.
CITY OF ROSEBURG
PUBLIC WORKS COMMISSION SPECIAL MEETING
JANUARY 23, 2020
MINUTES

CALL TO ORDER: The special meeting of the City of Roseburg Public Works Commission was called to order at 9:00 a.m. Thursday, January 23, 2020 in the Third Floor Conference Room at City Hall.

ROLL CALL: Present: Chair Bob Cotterell, Commissioners Pat Lewandowski, Roger Whitcomb, John Seward, Stuart Liebowitz, and Fred Dayton

Absent: Noel Groshong, Vern Munion, and Ken Hoffine

Others Present: Angela Rogge, David Evans and Associate Consultant

Attending Staff: City Manager Nikki Messenger, Public Works Director Brice Perkins, Community Development Director Stuart Cowie, Communications Specialist Eric Johnson, Public Works Staff Jim Macariello, and Department Technician Chanelle Rogers

APPROVAL OF MINUTES: Commissioner Whitcomb moved to approve the minutes of the January 9, 2020 Public Works Commission meeting. Motion was seconded by Commissioner Lewandowski and approved with the following vote: Chair Cotterell and Commissioners Whitcomb, Liebowitz, Seward, Dayton, and Lewandowski voted yes. No one voted no.

Messenger introduced the new Public Works Director Brice Perkins to the commission. He recently worked for the City of Medford and has been here just over one week. Messenger said staff is looking forward to working with Perkins. Community Development Director Stuart Cowie introduced himself to the commission.

DISCUSSION ITEMS:

Transportation System Plan: Cowie informed the City has been working on updating the Transportation System Plan (TSP) for about three years with David Evans & Associate, there have been a couple delays in that period including a contract amendment which delayed the project an additional year. Cowie said David Evans and Associate Angela Rogge, has been working on the TSP since the beginning and was going to give presentation on what the TSP is and why one is needed. Rogge reported that the TSP is a blueprint for all modes of travel. It is a document to use to attract and secure funding for projects in the community. She said the update process started in 2016 with a kick-off meeting that included the Public Advisory Committee (PAC). There was a gap in the process while five intersections were re-reviewed. She advised in the last year they have met with the PAC quite a few times. Rogge said five goals were set at the beginning of this process those being

- Mobility and Accessibility
- Vibrant Community
- Transportation Options
- Economic Vitality
- Implementation

Rogge informed the planning area includes city limits and the new Urban Growth Boundary area, there are 76 intersections to study in these areas and mostly are arterials/collectors. Some of these intersections are ODOT jurisdiction so the City can only make suggestions but ultimately it is ODOT that decides what changes are made on those particular intersections. Commissioner Seward
questioned how far ODOT jurisdiction extends at those intersections. Rogge said it is about a quarter mile each direction of each intersection so example the Garden Valley Blvd intersections with I-5 extend west to Stewart Parkway and East to NE Stephens. Chair Cotterell asked who would be paying for the changes at the ODOT intersections. Messenger said they would probably ask for federal funding but also the City would contribute some match since it does help with the grant process. Rogge said her company looked at a lot of different data and had meeting with the PAC to discuss the project list and which ones to have on the list. Rogge informed there were 27 projects that made the Tier 1 list which is projects that have a reasonable likelihood of being funded with existing sources and 58 projects on the Tier 2 list which are ones that would require new funding sources for implementation. Cowie said not all the funding is available currently, this is projected over the next 20 years so will need to prioritize the projects. It was mentioned the state wants City's to have TSP's to show that they are thinking of how to make improvements. Dayton questioned how all the new apartment complexes that are being constructed east of town play into the transit portion. Rogge said the transit district will work with the City on new routes if needed. Cowie also mentioned that when the City receives site review applications the transit district is contacted by staff. Messenger also stated the developers are at times asked to provide transit stops at the location they are developing. It was mentioned that a lot of the Bicycle/Pedestrian projects are focused in the UR area, and also to improve the existing trail system. Liebowitz stated the bike/walk group didn't feel that it was represented well so they will be attending the City Council meeting to voice their concerns. Rogge said the TSP doesn't prevent the city from doing other bike/pedestrian updates. Messenger also mentioned that some of the items that were on the bike/walk groups list are not projects that would be included in the TSP. Cowie said this plan included more bicycle/pedestrian projects then a typical TSP does. Discussion ensued. Dayton inquired if the intersection of SE Stephens and Diamond Lake Blvd will be able to handle the additional traffic with the new apartments that are being built east of town. Rogge replied that no it will not and that ODOT is aware but it is a very large project. She mentioned that is improvements are made to Douglas Ave or business come this side of town it will help with traffic since they won't need to cross town to get products.

**MOTION:** Commissioner Whitcomb moved to recommend the City Council adopt the Roseburg Transportation System Plan. Motion was seconded by Commissioner Seward and approved with the following vote: Chair Cotterell and Commissioners Dayton, Whitcomb, Munion, and Lewandowski voted yes. Liebowitz voted no.

**AUDIENCE PARTICIPATION:** None

**INFORMATIONAL ITEMS:** None

**BUSINESS FROM THE COMMISSION:** None

**NEXT MEETING DATE:** February 13, 2020

**ADJOURNMENT:** Meeting adjourned at 10:14

[Signature]

Chanelle Rogers, Public Works Department Technician
DATE: February 3, 2020
TO: Public Works Commission
FROM: Daryn Anderson, P.E.
VIA: Brice Perkins, P.E., Public Works Director
SUBJECT: Standby Generator Evaluation Study
Project No. 20WA03

ISSUE STATEMENT AND SUMMARY
The City has several critical facilities that currently do not have permanent standby power installed that would provide power in the event of an outage. The City contracted with a consultant to analyze critical facilities and provide a Standby Generator Evaluation Study. The issue for the Commission is whether to recommend that staff program resources in order to proceed with design and construction of permanent standby power at any or all eight of the facilities identified in the study.

BACKGROUND/ANALYSIS
Between February 23 and 26, of 2019 the City of Roseburg and much of greater Douglas County experienced a large scale snow storm that paralyzed much of Douglas County. As a result, much of Roseburg and the surrounding areas of the County experienced wide spread power outages and road closures due to downed trees and power lines from heavy wet snow. Outages lasted anywhere from a few hours to several days, depending on location. In many instances, residences in the elevated areas of the City and those in surrounding rural areas were without power for up to several weeks. Roseburg City Hall, the Public Works Maintenance Facility (Fulton Shop), the Winchester Water Treatment Plant (WTP), and some of the City's water booster pump stations lost power for approximately 30 hours. Some City booster pump stations lost power from four to seven days.

Historically, power outages occurring at more than two sites simultaneously has been a rare occurrence. The WTP has a dedicated power circuit that feeds directly from the adjacent Pacific Power substation. Generally, when a power outage does occur at the WTP it gets restored quickly and power interruption is short. The City of Roseburg has approximately one (1) day of water storage available in the main pressure zone reservoirs. During the February 2019 power outage, the WTP was unable to produce water and storage capacity was depleted to approximately 50 percent.

The PW Commission directed City staff to have a study completed that would include recommendations for standby power generation at the WTP and other key facilities in Roseburg. In August of 2019, the City contracted with RH2 Engineering Inc. to do a study. City staff identified seven locations that are critical to providing water for the City and to maintain supervisory control and data acquisition (SCADA) communication using the City's radio network. Staff also asked RH2 to evaluate the Fulton Shop Facility since it is where the
City's fueling facility is located and is critical for responding in the case of an emergency. The Fulton Shop also houses the City's backup computer server system.

Facilities evaluated in this report include:

1. Winchester Water Treatment Plant
2. Public Works Maintenance Shop
3. Reservoir Hill
4. Dixonville Pump Station No. 2
5. Garden Valley Pump Station
6. Hawthorne Pump Station
7. Kline Pump Station
8. Ventra Pump Station

The consultant looked at two primary types of fuel systems, dual-fuel (natural gas or propane), and diesel. The attached report addresses the advantages and disadvantages and operating costs for both systems. The cost estimates summarized below report are based on diesel generators.

The consultant looked at three design alternatives for each facility as follows:

**Alternative 1:** Install a permanent standby generator capable of operating at minimum electrical load to maintain operation at the facility.

**Alternative 2:** Install a permanent standby generator capable of operating at typical electrical load operated at the facility.

**Alternative 3:** Install a generator receptacle to allow use of a portable, trailer mounted generator at each site.

### Generator Sizing Summary

<table>
<thead>
<tr>
<th>Facility</th>
<th>Alternative 1 (Min.)</th>
<th>Alternative 2 (Typ.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dixonville Pump Station No. 2</td>
<td>25 kW</td>
<td>50 kW</td>
</tr>
<tr>
<td>Garden Valley Pump Station</td>
<td>150 kW</td>
<td>150 kW</td>
</tr>
<tr>
<td>Hawthorne Pump Station</td>
<td>150 kW</td>
<td>150 kW</td>
</tr>
<tr>
<td>Kline Pump Station</td>
<td>50 kW</td>
<td>50 kW</td>
</tr>
<tr>
<td>Ventura Pump Station</td>
<td>80 kW</td>
<td>80 kW</td>
</tr>
<tr>
<td>Reservoir Hill</td>
<td>N/A</td>
<td>30 kW</td>
</tr>
<tr>
<td>Public Works Maintenance Shop</td>
<td>450 kW</td>
<td>800 kW</td>
</tr>
<tr>
<td>Winchester WTP</td>
<td>900 kW</td>
<td>1500 kW</td>
</tr>
</tbody>
</table>
Permanent Generator Construction Cost Summary

<table>
<thead>
<tr>
<th>Facility</th>
<th>Alternative 1 (Min.)</th>
<th>Alternative 2 (Typ.)</th>
<th>Alternative 3</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dixonville Pump Station No. 2</td>
<td>$108,000</td>
<td>$125,000</td>
<td>$28,000</td>
</tr>
<tr>
<td>Garden Valley Pump Station</td>
<td>$153,000</td>
<td>$153,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Hawthorne Pump Station</td>
<td>$166,000</td>
<td>$166,000</td>
<td>$37,000</td>
</tr>
<tr>
<td>Kline Pump Station</td>
<td>$124,000</td>
<td>$124,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Ventura Pump Station</td>
<td>$131,000</td>
<td>$131,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Reservoir Hill</td>
<td>N/A</td>
<td>$111,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Public Works Maintenance Shop</td>
<td>$406,000</td>
<td>$619,000</td>
<td>N/A</td>
</tr>
<tr>
<td>Winchester WTP Total</td>
<td>$1,046,000</td>
<td>$1,334,000</td>
<td>N/A</td>
</tr>
<tr>
<td>Site Work</td>
<td>$77,000</td>
<td>$77,000</td>
<td></td>
</tr>
<tr>
<td>Power Equipment</td>
<td>$245,000</td>
<td>$245,000</td>
<td></td>
</tr>
<tr>
<td>Generator and ATS</td>
<td>$656,000</td>
<td>$944,000</td>
<td></td>
</tr>
<tr>
<td>Conduit and Wire</td>
<td>$53,000</td>
<td>$53,000</td>
<td></td>
</tr>
<tr>
<td>Control Panel</td>
<td>$15,000</td>
<td>$15,000</td>
<td></td>
</tr>
</tbody>
</table>

Note: Alternative 3 costs only include site improvements. Generators are not included in costs.

Portable Generator Cost Summary

<table>
<thead>
<tr>
<th>Portable Generator Size</th>
<th>Approximate Cost</th>
</tr>
</thead>
<tbody>
<tr>
<td>50 kW</td>
<td>$113,000</td>
</tr>
<tr>
<td>80 kW</td>
<td>$122,000</td>
</tr>
<tr>
<td>150 kW</td>
<td>$129,000</td>
</tr>
</tbody>
</table>

Multiple project scenarios are possible. Summarizing the engineer’s recommendations, the following options show estimated costs for four alternative scenarios:

Option #1 - **Backup power to all eight facilities**
- Water Treatment Plant (Alt #2, 1500 KW Generator) - $1,334,000
- Reservoir Hill (Alt 2, 30 KW Generator) - $111,000
- Generator Receptacle at 5 locations (Alt #3) - $137,000
- Portable Generators (2 EA, 150 KW) - $258,000
- Fulton Shop (Alt #1, 450 KW) - $406,000

Subtotal Option #1 $2,246,000

Option #2 - **Backup power to seven facilities**
- Water Treatment Plant (Alt 2, 1500 KW Generator) - $1,334,000
Reservoir Hill (30 KW Generator) - $ 111,000
Generator Receptacle at 5 locations (Alt 3) - $ 137,000
Portable Generators (2 EA, 150 KW) - $ 258,000

Subtotal Option #2 $ 1,840,000

Option #3 - **Backup power to WTP and Reservoir Hill only**
Water Treatment Plant (Alt 2, 1500 KW Generator) - $ 1,334,000
Reservoir Hill (30 KW Generator) - $ 111,000

Subtotal Option #2 $ 1,445,000

Option #4 - **Backup power to WTP only**
Water Treatment Plant (Alt 2, 1500 KW Generator) - $ 1,334,000

**FINANCIAL/RESOURCE IMPACTS**
Financial impacts range from $0 to $2,246,000 depending on the option chosen. Staff recommends that Option #3, with an estimated cost of $1,445,000, be included in the FY 20-21 Water Capital Fund budget.

**TIMING ISSUES**
The City currently operates without standby power generation at the above facilities. If a power outage occurs at the WTP the City is unable to produce water and must rely on limited storage in the reservoirs. Following the recent disastrous forest fires in California, in 2019 Pacific Power contacted the City to make us aware that customers in southern Oregon may be included in future rolling blackouts during periods of severe fire weather if high risk situations are present and the WTP is located in one of the zones.

In order to proceed with design and construction, it will be important to define which, if any, alternatives the Commission recommends staff move forward at this time.

**COMMISSION OPTIONS**
The Commission has the following options:
1. Recommend that staff program resources to proceed with design and construction of Option 1; or
2. Recommend that staff program resources to proceed with design and construction of Option 2; or
3. Recommend that staff program resources to proceed with design and construction of Option 3; or
4. Recommend that staff program resources to proceed with design and construction of Option 4; or
5. Recommend that staff not move forward with the project at this time; or
6. Request additional information.

**STAFF RECOMMENDATION**
Given the potential negative impacts of not having permanent standby power installed at critical facilities, staff recommends moving forward with a project. If the City wishes to maintain the operation and integrity of critical facilities and water system including its supervisory control and data acquisition system (SCADA) during times of natural disaster and inclement weather, Option #1 would be required.
In order to provide a minimum level of water production and SCADA monitoring, staff recommends proceeding with Option #3 to proceed with design and construction of permanent diesel powered standby power generation at the WTP and Reservoir Hill. While natural gas is a less expensive fuel, diesel is the recommended fuel option because diesel generators have a lifespan 3 to 4 times that of natural gas generators and provide the lowest lifecycle cost. Option #3 provides minimal water production to approximately 80% of the City’s customer base.

Any option selected will necessitate revision of the 2018 CIP.

**SUGGESTED MOTION**

*I move to recommend that staff proceed with design and construction of permanent standby power at the Water Treatment Plant and Reservoir Hill and the associated modification to the 2018 CIP*

**ATTACHMENTS**

A) Standby Generator Evaluation Study – Revision 1 (Pages 1-10)
STANDBY GENERATOR EVALUATION

Prepared for the City of Roseburg

Revision 1

January 2020

ROS 119.111

Prepared by:
RH2 Engineering, Inc.
22722 29th Drive SE, Suite 210
Bothell, WA 98021
(425) 951-5400
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City of Roseburg
Standby Generator Evaluation
January 2020

Prepared by RH2 Engineering, Inc.
Prepared for the City of Roseburg

Note: This evaluation was completed under the direct supervision of the following Licensed Professional Engineers registered in the State of Oregon.

Sincerely,

RH2 ENGINEERING, INC.

Expires: 12/31/2020
Signed: 1/17/2020
City of Roseburg
Standby Generator Evaluation
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Table 2 – WTP Electrical Loads – Alternative 1 and 2
Table 3 – Permanent Generator Construction Cost Summary
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Appendix A – Generator Sizing Reports
Appendix B – Generator Site Plans
Appendix C – Facility One-Line Diagrams
Appendix D – Detailed Cost Estimates
City of Roseburg
Standby Generator Evaluation
Generator Study

Introduction

The City of Roseburg (City) has several critical facilities that currently do not have permanent standby power installed that would provide power in the event of an outage. Maintaining power to each of these facilities is critical to both provide water for the City and maintain supervisory control and data acquisition (SCADA) communications throughout the City’s radio network. The City wishes to maintain the operation and integrity of its water system during times of natural disaster and inclement weather. RH2 Engineering, Inc., (RH2) has conducted site visits to document the existing facilities and prepare recommendations for the installation of standby generator systems at each facility. The facilities evaluated in this report consist of:

1. Winchester Water Treatment Plant
2. Public Works Maintenance Shop
3. Reservoir Hill
4. Dixonville Pump Station No. 2
5. Garden Valley Pump Station
6. Hawthorne Pump Station
7. Kline Pump Station
8. Ventura Pump Station

Several alternatives for each facility have been provided; these alternatives will be referenced throughout this evaluation. A summary of each alternative is as follows:

**Alternative 1**: Install a permanent standby generator capable of operating the minimum electrical load to maintain operation of the facility. Individual loads were identified by the City for the Water Treatment Plant (WTP) and Public Works Maintenance Shop. Minimum electrical load at the pump stations is defined as the lighting/heating load and a single booster pump operating.

**Alternative 2**: Install a permanent standby generator capable of operating the typical electrical load operated at the facility. Individual loads were identified by the City for the WTP and Public Works Maintenance Shop. Typical electrical load at the pump stations is defined as the lighting/heating load and all booster pumps operating.

**Alternative 3**: Install a generator receptacle to allow the use of a portable, trailer-mounted generator at each site. The receptacle would be sized to operate all electrical load, but functionality would depend on the size of generator provided.
Electrical Load Study and Generator Size Verification

All facilities except for Reservoir Hill contain a 277/480 Volts Alternating Current (VAC) three-phase power service; Reservoir Hill’s utility power service is 120/240 VAC single-phase. A thorough examination of each facility was performed, and individual electrical loads were documented and categorized. Pump motor starters, pump motor full load amperages, and lighting transformer sizes were recorded and modeled. Beyond nameplate information, there are other parameters that must be evaluated when sizing a generator. Inrush current is used to describe the instantaneous input current drawn by an electrical device when that device is first energized. Equipment such as rotating motors, transformers, lighting ballasts, and welders are examples of devices that traditionally have high inrush current. As the device energizes it can draw much higher amperage than what it consumes while operating; therefore, these items must be examined and accounted for carefully.

When sizing a generator, the inrush current can place more strain on the generator than the full-load operation of the facility. Due to Ohm’s law, one can assume that as this current increases, the power source would naturally decrease the output voltage. This balance can be measured by monitoring the voltage dip of the generator. Perhaps the most strain a generator will endure is the inrush current of a pump motor that is started across-the-line. The nature of this type of starter places the full inrush current of the motor on the generator, and that is where the largest voltage dip will occur. Traditionally, RH2 places a 15-percent voltage dip threshold on facilities; however, the 15-percent voltage dip is sometimes not feasible as it results in such an excessively sized generator that the cost is impractical. In those situations, RH2 evaluates the maximum permissible voltage dip on a site by site basis to make a reasonable assumption and recommendation. However, it should be noted that at sites with a voltage dip in excess of 15 percent, there may be the need to install a small uninterruptible power supply (UPS) on the motor starter control circuit to assist in smooth operation of the facility.

Another critical factor in sizing a generator is the total harmonic distortion (THD) of various electrical loads. THD is the parameter used to quantify the ratio of the sum of the harmonic components of a given signal by the power of the fundamental frequency. THD helps characterize an electrical system’s linearity, which is significant due to a generator’s limited ability to cope with the distortion. Devices such as computer power supplies and lighting ballasts contribute to the measurable THD on an electrical system.

Cummins Power Suite (May 2019 Release) generator sizing software was used to compile the electrical loads and determine generator sizing. Table 1 shows a summary of the generator sizes identified for the various alternatives at each site, as well as the simulated voltage dip. Appendix A includes the specific generator sizing reports for each site and each alternative.
Table 1  
Generator Sizing Summary

<table>
<thead>
<tr>
<th>Facility</th>
<th>Alternative 1 (Min.)</th>
<th>Alternative 2 (Typ.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dixonville Pump Station No. 2</td>
<td>25 kW</td>
<td>50 kW</td>
</tr>
<tr>
<td>Garden Valley Pump Station</td>
<td>150 kW</td>
<td>150 kW</td>
</tr>
<tr>
<td>Hawthorne Pump Station</td>
<td>150 kW</td>
<td>150 kW</td>
</tr>
<tr>
<td>Kline Pump Station</td>
<td>50 kW</td>
<td>50 kW</td>
</tr>
<tr>
<td>Ventura Pump Station</td>
<td>80 kW</td>
<td>80 kW</td>
</tr>
<tr>
<td>Reservoir Hill</td>
<td>N/A</td>
<td>30 kW</td>
</tr>
<tr>
<td>Public Works Maintenance Shop</td>
<td>450 kW</td>
<td>800 kW</td>
</tr>
<tr>
<td>Winchester WTP</td>
<td>900 kW</td>
<td>1500 kW</td>
</tr>
</tbody>
</table>

It is important to note is that there is no Alternative 1 scenario for Reservoir Hill due to the type of facility it is. None of the electrical loads at the site are controlled or switched and it is impractical to assume that any portion of the electrical load would not be operating at any given time.

The most complex facility evaluated in this report is the Water Treatment Plant. Table 2 summarizes the electrical loads the generator is sized for under each alternative. The motor loads that have the largest impact between the two alternatives are the high service pumps and the intake pumps. In Alternative 1 only one intake and high service pump would be allowed to run whereas two intake and high service pumps are allowed to run in Alternative 2. Therefore, Alternative 2 allows the plant to produce more water on standby power. The intake and high service pumps are two of the largest electrical loads at the plant, so adding these loads in alternative 2 has a significant impact on the generator size and cost of the project.
## Table 2
### WTP Electrical Loads – Alternative 1 and 2

<table>
<thead>
<tr>
<th>Electrical Load</th>
<th>Alternative 1 (Min.)</th>
<th>Alternative 2 (Typ.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Panel LA and LB</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Panel 4A00</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>High Service Pump No. 3</td>
<td></td>
<td>X</td>
</tr>
<tr>
<td>High Service Pump No. 4</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Exhaust Fan EF-1</td>
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<td>X</td>
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<tr>
<td>Exhaust Fan EF-2</td>
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<td>X</td>
</tr>
<tr>
<td>Sludge Collector Drive</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Sludge Transfer Valve Actuator</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Flocculator Motor E1</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Flocculator Motor E2</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Flocculator Motor E3</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Rapid Mixer No. 1</td>
<td>X</td>
<td>X</td>
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<tr>
<td>Backwash Pump No. 1</td>
<td></td>
<td>X</td>
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<tr>
<td>Air Compressor</td>
<td>X</td>
<td>X</td>
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<tr>
<td>Blower</td>
<td>X</td>
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<tr>
<td>Wastewater Pump No. 1</td>
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<td>X</td>
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<tr>
<td>Wastewater Pump No. 2</td>
<td></td>
<td>X</td>
</tr>
<tr>
<td>Storage Building Distribution Panel</td>
<td></td>
<td>X</td>
</tr>
<tr>
<td>Intake Pump No. 2</td>
<td></td>
<td>X</td>
</tr>
<tr>
<td>Intake Pump No. 3</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Traveling Screen No. 1</td>
<td>X</td>
<td>X</td>
</tr>
<tr>
<td>Panel LD</td>
<td>X</td>
<td>X</td>
</tr>
</tbody>
</table>

### Fuel System Evaluation

There are two primary types of fuel systems used for standby generators of the size considered in this evaluation: 1) dual-fuel (gaseous), and 2) diesel. A dual-fuel (gaseous) generator has the ability to operate using either natural gas or propane fuel. The most common type of fuel is diesel, compromising nearly 90 percent of the market share, yet there are certain scenarios where it makes sense to utilize a dual-fuel generator instead.

A diesel generator typically uses a local fuel tank either located directly beneath the generator (commonly referred to a sub-base fuel tank) or in a separate above-ground fuel tank. Sub-base fuel tanks provide decreased costs but are limited in size. Where a fuel supply exceeds the capacity limitations of the sub-base configuration, a separate standalone fuel tank must be provided. The cost of a separate fuel tank far exceeds that of the sub-base tank due to the necessary infrastructure needed to support the fuel tank. A dedicated equipment pad along with underground fuel piping, transition sumps, and leak containment must be provided with
an above-grade fuel tank. Typically, an alarm panel is provided at the fuel tank for both leak detection alarming and overfill prevention. With the City’s desired 48-hour fuel supply, sub-grade fuel tanks can be provided for all sites except the Winchester WTP and the Public Works Maintenance Shop.

A dual-fuel generator can operate using either natural gas or propane. Natural gas, provided by means of a utility connection, fuels the generator when available, while a separate propane tank serves as a local backup supply of local fuel in the event of a disturbance in the utility supply of natural gas. The generator is able to detect whether the supply of natural gas is present and is capable of automatically switching to the reserve propane supply as necessary.

Diesel generators typically are advertised as having a 20,000-hour lifespan, along with excellent reliability in cold weather. The engines are industrial in nature, with low piston speed, and are designed for longevity and maintainability. Diesel fuel itself has a shelf life of 18 to 24 months, but this can be extended by using additives or by having a third-party fuel polishing service performed to remove impurities from the supply. Diesel generators are subject to “wet stacking” if they are underutilized, a phenomena where unburnt fuel can cling to the interior of the exhaust system, but this should not be an issue for this specific installation as the generators considered are not oversized.

Dual-fuel generators typically are advertised as having a 5,000- to 6,000-hour lifespan due to their commercial grade engines. Dual-fuel generators are cleaner burning, with very little soot or carbon tracking near the exhaust. Propane has the added benefit of up to a 10-year shelf life of the local supply, mitigating the concern of fuel growing stale that exists with diesel. One considerable shortcoming of a dual-fuel generator is the inability to store a fuel supply in large quantity compared to an equivalent diesel generator. Due to the stringent requirements of large propane tanks, it is not advisable or cost effective to install a local fuel tank larger than 1,000 gallons. With the generator sizes considered as part of this study, the limitations of the fuel tank size limit the potential operating time if the generator were to rely solely on the local storage. Additionally, the fuel plumbing and leak detection requirements are more stringent, which can drive up construction costs. However, there are convenience benefits, as using a utility-provided natural gas supply lessens the need to monitor local fuel storage tank levels and top off as needed.

There are advantages and disadvantages to either fuel system; all of which play a role in determining which equipment best suits a project’s needs. To accurately convey the differences between the two generators, it is wise to consider not just the technical performance of a single generator but the practical availability and performance of the common suppliers of generators. Due to their popularity, the availability of diesel generators in a variety of sizes is abundant, creating a competitive bidding atmosphere. However, the same cannot be said of dual-fuel generators; while there are multiple suppliers, the sizes between suppliers are not as standardized as their diesel counterparts. Due to the lessened availability, the bidding process can favor one supplier over another if the sizing of the generator does not strike a number that multiple manufacturers can provide.

Operating costs between the two systems vary as both efficiency and fuel prices fluctuate. For two generators of similar size, the fuel costs to operate a unit on natural gas are approximately
50 percent of those required to operate a same-sized diesel generator. However, if the
dual-fuel unit must rely on the local propane fuel supply, the operating costs of the unit are
nearly 400 percent of the equivalent diesel generator.

With a diesel generator there is a concern with very large fuel tanks that fuel may exceed its life
expectancy if it goes unused and is not properly maintained. This would only be a concern at
the Winchester Water Treatment Plant. One potential remedy to this problem is to add a fuel
dispenser to a diesel tank, which would allow the City to fill vehicles and/or equipment with the
on-site diesel. The benefit of this is that it both serves to cycle fuel quicker and provides an
emergency source of diesel fuel during times of natural disaster. One pitfall of installing the
dispenser is that if the fuel is used in road-going vehicles then the tank must be filled with
road-taxed fuel, which is considerably more expensive than off-road diesel fuel that could
otherwise be used for the generator. It is estimated that to add a fuel dispenser to a fuel tank
would add approximately $10,000 to the total construction cost of the project.

There are several types of above-grade diesel fuel tanks available for diesel generator
applications. The most common tank is a UL-142 style, which consists of a mild steel
double-walled tank with spill prevention. Some owners elect to install a UL-2085 tank, which is
very similar but includes an additional layer within the tank designed to provide protection
against the tank breaking or severing in the event of a vehicle collision and against fire
exposure. The cost estimates provided for the Winchester Water Treatment Plant and Public
Works Maintenance Shop assume that a UL-142 tank is provided; to upgrade to a UL-2085 fuel
tank it is estimated to add approximately $8,000 per fuel tank but can vary based on capacity.

Sound Attenuation Evaluation

Sound attenuation is important to ensure that the generator installation is as least disruptive to
both the facility and the neighbors as possible. For the purpose of this study, all generators are
assumed to include an outdoor-rated sound-attenuated enclosure that will restrict noise to no
more than 75 decibels (dB) as measured 23 feet from the generator. This is the most
sound-attenuated industry standard enclosure available. Additional sound attenuation is
available but requires custom fabrication and is significantly more expensive. It is estimated
that to reduce to a 65 dB enclosure would add approximately $15,000 to each pump station
generator, and approximately $40,000 to either the Public Works Maintenance Shop or
Winchester Water Treatment Plant generator.

The City of Roseburg Code of Ordinances addresses noise concerns in Chapter 7.02 – Offense.
Exemption B of 7.02.140 – Noise Disturbances states, “The use of emergency equipment
required to protect life or property.” After visiting each site, RH2 did not identify any locations
where noise attenuation beyond the standard 75 dB is warranted.

Site and Security Evaluation

Generator location is a critical element of overall standby generator power design. The selected
location must be secure from vandalism while providing adequate access for maintenance and
fueling. Additionally, the generator must maintain fire code mandated clearances from
buildings and other structures. Individual site plan schematics have been prepared for each facility and can be found in Appendix B. A summary of the design constraints and overall site preferences has been prepared for each site.

**Dixonville Pump Station No. 2**

The pump station is located in a rural area, where vandalism is less of a concern. The existing property has vehicle access via a driveway, with a landscaped area at the edge of the driveway. Locating the generator in the landscaped area places it adjacent to the building, minimizing site work costs. It also makes it easily accessible for re-fueling.

**Garden Valley Pump Station**

The pump station is located in a neighborhood, surrounded by residential homes. There is no existing site security fence. The property is covered in trees, which would need to be trimmed and/or removed to place the generator. The proposed location of the generator is to the northwest of the pump station building.

**Hawthorne Pump Station**

The pump station is located in a neighborhood, surrounded by residential homes. There is no existing site security fence. The slope of the site limits potential generator locations due to inaccessibility. The proposed location is to the north of the building, along the existing driveway.

**Kline Pump Station**

The Kline Pump Station is surrounded by a security fence. The pump station building lies adjacent to a water reservoir on the site. When evaluating generator locations, it appeared that placing it behind the pump station would not impact site accessibility, while also providing room to service and fuel the generator.

**Ventura Pump Station**

The pump station is surrounded by residential homes. There is no existing site security fence. The existing property has limited street access, limiting potential locations for the generator. The proposed location is to the west of the building.

**Reservoir Hill**

Reservoir Hill is surrounded by a security fence but is also prone to foot traffic. The overall site is large, with plenty of room to place the generator. The selected location puts the generator near the existing power service entrance, which will help reduce site work costs. The generator lies outside of the access road surrounding the reservoir.

**Public Works Maintenance Shop**

The Maintenance Shop is surrounded by driveways and parking lots. Much of the existing space along the perimeter of the site has been utilized for material storage. The proposed location places the generator alongside the fence, with the separate fuel tank beside it. The location allows for access to the generator without inhibiting vehicle traffic around the building.

**Winchester Water Treatment Plant**
The water treatment plant is surrounded by a security fence with several grassy areas beside the filter basins. The overall size of the generator and fuel tank can be accommodated by several locations on the site. The selected location places the generator near the existing power service and maintains easy accessibility for fueling and maintenance. The location also leaves room for a potential filter upgrade in the future.

**Electrical System Upgrades Summary**

Integrating a generator, either permanently or using a receptacle, requires the use of a transfer switch. The transfer switch allows the facility load to be powered by either the utility transformer or the generator. Typically, a permanent generator requires an automatic transfer switch, meaning that the facility can call the generator to operate and switch to the backup power supply autonomously. With a portable generator, a manual transfer switch is typically provided, which requires a user to physically operate the switch. In either instance the switch can be installed indoors or outdoors, depending on user preference. It is recommended to place an automatic transfer switch indoors where possible to extend its lifespan. With a manual transfer switch, it is recommended to place it outdoors near the receptacle for easier operation by the end-user. With either switch the electrical installation is similar; the service conductors must be intercepted and routed through the switch and then the switch is connected to the load. At some facilities, with a standalone service entrance switch, this is simpler, and at others it requires providing a new service disconnect switch. Preliminary one-line diagrams have been prepared to show the integration of an automatic transfer switch at each facility. The diagrams can be found in Appendix C. The one-lines remain relevant for both Alternative 1 and Alternative 2. In the case of Alternative 3 the automatic transfer switch would be replaced with a manual transfer switch, and the proposed generator would be replaced with a generator receptacle. Wiring would remain the same for Alternative 3 as the other scenarios.

The one-line diagrams indicate whether the switches would be placed indoors or outdoors, based on observations during the site visits. Final transfer switch location would be revisited during design to optimize user functionality and City preference.

Significant electrical work is necessary at the WTP due to the size of the electrical service. The existing switchboard cannot accommodate an automatic transfer switch; therefore, a new outdoor service disconnect in a switchboard is necessary to protect the line side of the transfer switch. The transfer switch itself would need to be installed in an outdoor enclosure adjacent to the new service disconnect. With the relocation of the disconnect a new grounding electrode system would need to be installed and bonded to the existing grounding grid. The equipment necessary to accommodate the 4000 Ampere (A) service entrance is extremely costly due to its size. A detailed phasing plan would be necessary to limit power outages at the site as much as possible, but it is expected that several short-term outages would be necessary to complete the installation.

**Projected Construction Cost Summary**

Construction costs have been prepared for each facility and for each subsequent alternative. Overall project costs account for the generator, transfer switch, site work, fuel supply, conduit,
and wire. Alternative 3 costs only include the materials and work necessary to provide a generator receptacle; they do not include the portable generators themselves. Alternative 3 costs have not been prepared for the WTP or Public Works Maintenance Shop, as a portable generator of the size necessary for the plant is not a feasible option for the City to own and operate and would not satisfy the City’s fuel supply requirements. Overall costs are summarized in Table 3.

### Table 3
Permanent Generator Construction Cost Summary

<table>
<thead>
<tr>
<th>Facility</th>
<th>Alternative 1 (Min.)</th>
<th>Alternative 2 (Typ.)</th>
<th>Alternative 3</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dixonville Pump Station No. 2</td>
<td>$108,000</td>
<td>$125,000</td>
<td>$28,000</td>
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<tr>
<td>Garden Valley Pump Station</td>
<td>$153,000</td>
<td>$153,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Hawthorne Pump Station</td>
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<td>$166,000</td>
<td>$37,000</td>
</tr>
<tr>
<td>Kline Pump Station</td>
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<td>$24,000</td>
</tr>
<tr>
<td>Ventura Pump Station</td>
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<td>$131,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Reservoir Hill</td>
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<td>$111,000</td>
<td>$24,000</td>
</tr>
<tr>
<td>Public Works Maintenance Shop</td>
<td>$406,000</td>
<td>$619,000</td>
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</tr>
<tr>
<td>Winchester WTP Total</td>
<td>$1,046,000</td>
<td>$1,334,000</td>
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</tr>
<tr>
<td><strong>Site Work</strong></td>
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<td></td>
</tr>
<tr>
<td><strong>Power Equipment</strong></td>
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<td>$245,000</td>
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<tr>
<td><strong>Generator and ATS</strong></td>
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<td>$944,000</td>
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<tr>
<td><strong>Conduit and Wire</strong></td>
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<td>$53,000</td>
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<tr>
<td><strong>Control Panel</strong></td>
<td>$15,000</td>
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</tr>
</tbody>
</table>

Note: Alternative 3 costs only include site improvements. Generators are not included in costs.

Detailed cost estimates for each facility have been prepared and can be found in Appendix D. Additionally, costs for the necessary portable generators to operate the facilities have been compiled in Table 4. Standard generator sizes were selected that would provide functionality at the booster pump stations and reservoir. Refer to Table 1 for the necessary generator size for each facility.

### Table 4
Portable Generator Cost Summary

<table>
<thead>
<tr>
<th>Portable Generator Size</th>
<th>Approximate Cost</th>
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</thead>
<tbody>
<tr>
<td>50 kW</td>
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<tr>
<td>80 kW</td>
<td>$122,000</td>
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<tr>
<td>150 kW</td>
<td>$129,000</td>
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</table>

The Federal Emergency Management Agency (FEMA) offers several generator reimbursement programs that may be applicable to the installation of one or more generators throughout the City. Specifically, the Hazard Mitigation Grant Program and Pre-Disaster Mitigation Program
City of Roseburg
Standby Generator Evaluation

offer up to 75-percent reimbursement programs for qualifying generator installations. These programs exist to fund permanent generators, portable generators, and improvements necessary for generator receptacles. Applications for each site would need to be prepared and submitted to FEMA for evaluation and potential approval.

Recommendations

To provide the Alternative 1 generator option at all five pump stations would total $768,000; Alternative 2 generators drive this cost up to $788,000. In comparison, to provide generator receptacles at all five pump stations and provide two portable 150 kilowatt (kW) generators would total $411,000. It is unlikely that power outages will occur at more than two sites simultaneously. With the reservoir storage capacity of the City it is likely that portable generators could be rotated throughout the sites to maintain an operable situation until utility power has been restored at one or more sites. RH2 recommends that the City install portable generator receptacles (Alternative 3) at all five pump stations. Additionally, RH2 recommends that the City procure two 150 kW portable generators.

Reservoir Hill is a critical site due to its critical role in the radio communications of the City’s supervisory control and data acquisition (SCADA) system. A power outage at Reservoir Hill results in the loss of the City to remotely monitor all of the City’s water facilities. Because of the important role this site plays in the SCADA system it is recommended to install the Alternative 2 generator at Reservoir Hill.

At the Public Works Maintenance Shop it is likely that actual observed load is substantially lower than the load calculations would indicate. The overall use and function of the Maintenance Shop is such that electrical loads could be manipulated to avoid overloading the generator. RH2 recommends the Alternative 1 generator option at the Public Works Maintenance Shop.

When comparing the overall costs of the Alternative 1 and Alternative 2 generators at the Winchester Water Treatment Plant, it is apparent that there is only a 22 percent savings associated with Alternative 1. Due to the critical nature of the treatment plant and the potential for future expansion, the Alternative 2 generator is recommended for the Winchester Water Treatment Plant.