## TM\#3: CURRENT TRANSPORTATION SYSTEM OPERATIONS

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Project \#: 23021.032
To: Project Management Team
From: Kittelson \& Associates, Inc., and HDR, Inc.
Subject: OR 138E Design Concept Plan

## Purpose

The purpose of this technical memorandum is to document the existing multimodal operations and safety conditions along the OR 138E study corridor and supporting local roadways. Specific study elements include the following:

- Existing pedestrian and bicycle network assessment;
- Existing transit network assessment;
- Existing multimodal safety assessment at the study intersections and study area roadway segments;
- Existing traffic conditions along the OR 138E study corridor and other key study area roadways;

The analyses summarized in this memorandum will serve as a baseline for identifying and evaluating potential solutions and developing a prioritized list of improvements for the OR 138E Design Concept Plan.

## Existing Pedestrian and Bicycle Network Assessment ${ }^{1}$

Pedestrian and Bicycle analyses were performed for roadway segments within the study area, including the OR 138E corridor between SE Douglas Avenue and the eastern Urban Growth Boundary (UGB). Other important parallel and perpendicular routes were also evaluated such as Douglas Avenue, Stephens Street, Winchester Street, and Jackson Street. The level of traffic stress $(\text { LTS })^{2}$ methodology provides a measure of perceived stress experienced while walking or biking next to traffic.

The assessment of the existing pedestrian and bicycle network within the study area was performed using the LTS methodology from ODOT's Analysis Procedures Manual Version 2 (APM). The APM classifies the experience for people walking into the following four Pedestrian Level of Traffic Street (PLTS) ratings:

- PLTS 1 represents low traffic stress and is suitable for most users including children. Typical locations have a wide sidewalk with low traffic speeds and/or a paved or landscaped buffer between the user and the travel lanes.
- PLTS 2 represents low traffic stress but requires more attention from users than PLTS 1 and is suitable for most users over 10 years old. Typical locations have sidewalks in good condition but may have higher speeds or traffic volumes than PLTS 1 segments.
- PLTS 3 represents moderate traffic stress and is suitable for most adults. Typical locations feature higher speeds and volumes and may have places that are challenging or impassible for wheeled mobility devices.
- PLTS 4 represents high traffic stress and is suitable only for able-bodied adults. Typical locations feature high traffic volumes and/or speeds. All streets without sidewalks fall into this category. All users should consider alternative routes.

The APM classifies the experience for people biking into the following four Bicycle Level of Traffic Street (BLTS) ratings:

- BLTS 1 represents low traffic stress and is suitable for most riders, including children. Speeds are low and there is only one travel lane per direction. Typical locations are local streets and separated bikeways.
- BLTS 2 represents low traffic stress but requires more attention than BLTS 1 and is suitable for most teens and adult riders. Typical locations are collector streets with bike lanes or central business districts.
- BLTS 3 represents moderate traffic stress and is suitable for most adult riders. Typical locations include arterials with low speeds and bike lanes and shared facilities with no more than one travel lane per direction.
- BLTS 4 represents high traffic stress and is only suitable for experienced and skilled riders. Typical locations are roadways with multiple lanes per direction and high speeds.

[^0]Each study roadway was split into segments reflecting changes in posted speed, functional classification, and other roadway characteristics likely to affect LTS ratings. The Recommended Urban Context of the corridor based on Oregon Department of Transportation's (ODOT) Highway Design Manual (HDM) and shown in Technical Memorandum 1 was also considered as a segmentation framework. The City's BLTS from the 2019 Transportation System Plan (TSP) was used as a reference, although there are slight changes to segment identification. The BLTS ratings for this analysis differ from the TSP for some segments as the APM was updated since the TSP was completed.

## Existing Pedestrian LTS

The APM sets a goal for PLTS ratings of 2 or better and PLTS ratings exceeding 2 should be identified as unfavorable for walking conditions. Table 1 and Figure 1 show ratings for segments in the study area. The majority of the segments ratings PLTS 3 or 4 . There are several key reasons for these results. On OR 138E, the lack of sidewalks east of Patterson Street and a lack of buffers such as bike lanes, on-street parking, or landscaping on the 5-lane western portion of OR 138E with posted speed of 35 miles per hour (mph) present unfavorable conditions for people walking along this corridor. Similarly, Douglas Avenue lacks sidewalks east of Ramp Road. The best ratings are found downtown centered around Jackson Street and on the western end of Douglas Avenue. Sidewalks are wider there and some include hard and landscaped buffers with trees. Speeds are lower, and the number of lanes is lower.

Some ratings are affected by the fact that certain sidewalk sections have effective widths of 2 feet or less due to the location of utility poles. Effective width is defined by the APM as the portion of the sidewalk that is clear of obstructions for pedestrians. This issue is particularly prevalent on the north side of OR 138E between Winchester Street and Casper Street. The issue is compounded by the fact that the right-of-way for much of OR 138E abuts existing structures and provides little to no room for roadway or sidewalk expansion. By comparison, the southern section of SE Stephens Street rates better (PLTS 3) due to wider sidewalks (7 feet) that are in good condition and adjacent to bike lane buffers. The 7 -foot effective width of the sidewalks was enabled, in part, by relocating utility poles off of the sidewalks.

## Existing Bicycle LTS

The BLTS analysis represented in Table 2 and in Figure $\mathbf{2}$ shows that streets in the study area rating as either BLTS 3 or 4 . The poorest ratings are along OR 138E, which has higher speeds, a higher number of lanes, and no bike lanes. Douglas Avenue rates as a 3 largely due to its relatively high traffic volume (Average Daily Traffic (ADT) of 3,000 ) for a collector street. Although Winchester Street has a bike lane, it rates poorly due to the narrow width of the bike lane (5 feet) and the posted speed ( 35 mph ). SE Stephens Street between OR 138E and Douglas Avenue rates poorly despite having a bike lane due to the number of motor vehicle travel lanes in each direction (3) and narrow bike lane width ( 5 feet).

Figure 1. Existing Pedestrian Level of Traffic Stress Ratings (Roadway Segments)


Figure 1

Figure 2. Existing Bicycle Level of Traffic Stress Ratings (Roadway Segments)


Figure 2

Table 1: Existing Pedestrian Level of Traffic Stress Ratings (Roadway Segments)

| Segment | Sidewalk Effective Widih (ft) | Sidewalk Condition | Buffer Type | Tołal Buffer Widith (ft) | Travel Lanes | Maximum Posted Speed Limit (mph) | HDM Urban Context | APM Reference Table | Existing Pedestrian LTS Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OR 138E <br> (NE Stephens St. to NE Pamona St.) | 2 | Fair | N/A | 0 | 5 | 45 | Commercial Corridor | 14-23 | 4 |
| OR 138E <br> (NE Pamona St. to Buckhorn Ra.) | 0 | N/A | N/A | 0 | 5 | 55 | Suburban Fringe | 14-21 | 4 |
| SE Douglas Ave. <br> (SE Stephens St. to SE Fowler St.) | 5 | Fair | Landscaped with Trees | 4 | 3 | 20 | Downtown/ CBD | 14-23 | 2 |
| SE Douglas Ave. <br> (SE Fowler St. to SE Ivy Ave.) | 5 | Fair | Parking | 7 | 2 | 25 | Residential Corridor | 14-23 | 2 |
| SE/NE Douglas Ave. <br> (SE Ivy Ave. to Deer Creek) | 5 | Fair | N/A | 0 | 2 | 35 | Residential Corridor | 14-22 | 3 |
| NE Douglas Ave. (Deer Creek to OR 138E) | 0 | N/A | N/A | 0 | 2 | 35 | Suburban Fringe | 14-21 | 3 |
| NE Stephens St. <br> (NE Winchester St. to OR 138E) | 5 | Fair | bike Lane | 5 | 5 | 35 | Commercial Corridor | 14-23 | 3 |
| SE Stephens St. <br> (OR 138E to SE Douglas Ave.) | 7 | Good | Bike Lane | 5 | 5 | 25 | Commercial Corridor | 14-23 | 3 |
| NE Winchester St. <br> (NE Stephens St. to OR 138E) | 5 | Fair | Bike Lane | 5 | 3 | 35 | Urban Mix | 14-23 | 3 |
| NE Jackson St. <br> (OR 138E to SE Douglas Ave.) | 5 | Fair | Landscaped with Trees, Parking | 11 | 2 | 25 | $\begin{aligned} & \text { Downtown } \\ & \text { CBD } \end{aligned}$ | 14-21 | 2 |

Table 2. Existing Bicycle Level of Traffic Stress Ratings (Roadway Segments)

| Segment | Functional Class | Bike Lane | Bike Lane Width | Lanes Per Direction | Maximum Posted Speed Limit | APM Reference Table | Existing Bicycle LTS Rating |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OR 138E <br> (NE Stephens St. to NE Pamona St.) | Arterial | N | 0 | 3 | 45 | 14-6 | 4 |
| OR 138E <br> (NE Pamona St. to Buckhorn Rd.) | Arterial | N | 0 | 3 | 55 | 14-6 | 4 |
| SE Douglas Ave. <br> (SE Stephens St. to SE Fowler St.) | Collector | N | 0 | 2 | 20 | 14-5 | 3 |
| SE Douglas Ave. (SE Fowler St. to SE Ivy Ave.) | Collector | N | 0 | 1 | 25 | 14-5 | 3 |
| SE/NE Douglas Ave. (SE Ivy Ave. to Deer Creek) | Collector | N | 0 | 1 | 35 | 14-6 | 3 |
| NE Douglas Ave. (Deer Creek to OR 138E) | Collector | N | 0 | 1 | 35 | 14-6 | 3 |
| NE Stephens St. <br> (NE Winchester St. to OR 138E) | Arterial | Y | 5 | 3 | 35 | 14-4 | 3 |
| SE Stephens St. <br> (OR 138E to SE Douglas Ave.) | Arterial | Y | 5 | 3 | 25 | 14-4 | 3 |
| NE Winchester St. (NE Stephens St. to OR 138E) | Collector | Y | 5 | 2 | 35 | 14-4 | 3 |
| NE Jackson St. (OR 138E to SE Douglas Ave.) | Local | N | 0 | 1 | 25 | 14-5 | 3 |

## Existing Pedestrian Crossings Analysis

ODOT's 2023 HDM provides guidance on pedestrian crossing target spacing for state highways based on the urban context. The recommended urban context for the OR 138E corridor from SE Douglas Avenue to Pomona Street, established in Technical Memorandum \# 1: Corridor Vision, Definitions, and Background, is Urban Mix, for which the HDM recommends a maximum spacing between crossings of no more than 550 feet.

The recommended urban context for the eastern end of the corridor from Pomona Street to the City's eastern UGB is Suburban Fringe, for which the HDM recommends up to 1,500 feet between crossings.

There are four marked pedestrian crossings along the state highways within the project study area:

- 1) Stephens Street/Douglas Avenue
- 2) OR 138E/Stephens Street
- 3) Winchester Street/Jackson Street/OR 138E, and
- 4) Rifle Range Street/OR 138E

Existing marked pedestrian crossing is summarized in Table 3.Each crossing location is signalized with marked crosswalks. The OR 138E crossing at Rifle Range Street is the only crossing in the 3.75 miles between Winchester Street and the eastern edge of the study area, resulting in lengthy gaps in the crossing network. Along OR 138E, the distance between Winchester Street and Rifle Range Street is approximately 1 mile, while the distance between Rifle Range Street and the study area's eastern end is 2.8 miles.

Roseburg's TSP proposes a new signalized crossing on OR 138E at either Fulton Street or Lake Street, which will decrease the distances between several crossings ( $\sim 2,500$ feet), but not enough to meet the recommended HDM guidelines ( 550 feet in this segment).

Table 3: Distances Between Existing Signalized Crossings in Study Area

| From | To | HDM Urban <br> Context | Recommended <br> Distances between <br> Crossings | Actual <br> Distance |
| :--- | :--- | :---: | :---: | :---: |
| SE Stephens St./ <br> SE Douglas Avenue | OR 138E/ <br> Stephens Street | Urban Mix | $250-550$ feet | 820 feet |
| OR 138E/ <br> NE Stephens Street | OR 138E/ <br> Winchester Street | Urban Mix | $250-550$ feet | 510 feet |
| OR 138E/ <br> NE Winchester Street | OR 138E/ <br> Rifle Range Street | Urban Mix | $250-550$ feet | 1 mile |
| OR 138E/ <br> NE Rifle Range Street | OR 138E/ <br> Buckhorn Road | Urban Mix, <br> Suburban Fringe | $250-550$ feet, <br> $750-1,500$ feet | 2.8 miles |

## Existing Transit Network Assessment

A Qualitative Multimodal Analysis (QMA) was performed for transit facilities in the project corridor. QMA analysis is consistent with APM guidance and suitable for available data. Bus stop infrastructure was evaluated based on existing physical conditions and transit service features such service hours and frequency were reviewed from the Umpqua Public Transportation Distric $\dagger$ (UPTD) Master Plan

There are three UPTD bus lines serving the study area: Roseburg Greenline, Roseburg Redline, and the Sunshine Park Route. The Greenline and Redline offer 1-hour service and the Sunshine Park Route has four arrivals between 7:30 AM and 7:00 PM. The Greenline is the major service line along OR 138E, while the end stop of the Sunshine Park Route is near the eastern edge of the study area. The Redline runs perpendicular, crossing the western edge of OR 138E along Winchester Street and Jackson Street, with several stops within a quarter mile of the study area.

The results of the QMA analysis can be found in Table 4. The two main study area transit routes (Greenline and Redline) feature hourly service and it is assumed that travel times and reliability are relatively consistent for each line. Accordingly, the QMA analysis focused on transit stop conditions such as shelters and marked signage, distances between transit stops and the nearest crossings, and the connecting pedestrian and bicycle environment. The QMA evaluation range for each transit stop is: Excellent, Good, Fair, Poor.

- Excellent is represented by stops that are marked with shelters and connected to a pedestrian network with a rating of PLTS 1 .
- Good is represented by stops that are marked and are connected to a pedestrian network with a rating of PLTS 1 or 2.
- Fair is represented by stops that are marked or have a shelter and are connected to a pedestrian network with a rating of PLTS 3 or 4.
- Poor is represented by stops that are not marked, do not have shelters, and are connected to a pedestrian network with a rating of PLTS 3 or 4.
- Bicycle facilities were considered as a limiting factor. For segments rated as BLTS 4, the highest transit rating available was Fair. For segments rated as BLTS 3, the highest transit rating available was Good.

Some transit stops have shelters while some are not marked. The PLTS ratings for the areas surrounding the transit stops range from PLTS 2 to 4. Bus stops rated as "Poor" reflect areas that are not pedestrian friendly and do not provide any shelter. Unmarked stops also fall into this category. Bus stops rated as "Excellent" represent high-quality transit treatments with marked shelters and a PLTS rating of 1 . While none of the current stops have an "Excellent" rating, there are several that could achieve this with minor improvements. The primary differentiation between "Good" and "Fair" is the split between PLTS ratings of 2 and higher. OR 138E has only one marked crossing between Winchester Street and the eastern edge of the study area. Stops that reside more than a quarter mile from the nearest formal crossing were downgraded one level in the QMA analysis. Some of these ratings could change when a signalized crossing is built at Fulton Street or Lake Street, as listed in the TSP.

Figure 3 Existing Transit Qualitative Multimodal Assessment Ratings (Transit Stops) and Signalized Crossings


Figure 3

The pedestrian environment strongly impacts the QMA ratings of transit stops. The transit stops rated as Fair and Poor are located on OR 138E, a street with a pedestrian rating of PLTS 4, whereas transit stops rated as Good are located on streets with pedestrian rating of PLTS 2. Several transit stops would rate better with relatively minor improvements such as markings or shelters. Other transit stops will be harder to improve ratings for because they are limited by long distances to crossings.

New housing continues to grow in Roseburg, potentially increasing the need for expanded transit service into new areas. One of the primary areas that is growing is the study area's northeastern area, where hundreds of new lower-income and market rate units are currently being built. The Greenline may need to fill in the service gap between Pomona St. and Sunshine Park with additional stops to serve a growing population. Another potentially growing area is the subdivision area south of Douglas Avenue between Ramp Road and Pearce Road. As this area fills in, there may be a greater need for direct access to transit on OR 138E between the Kowloon Restaurant and Phoenix School stops.

Table 4: QMA Ratings for Existing Study Area Transit Stops

| Route | Stop ID | Location | Marked | Shelter | BLTS | PLTS | Distance †o Nearest Crossing | Ratings |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Redline / Greenline | 44, 18 | Dairy Queen, Winchester Street | Y | N | 3 | 2 | 540 feet | Good |
| Greenline | 25 | Library, Fowler Street | Y | Y | 3 | 2 | 500 feet | Good |
| Greenline | 19 | 76 Gas Station, OR 138E | N | N | 4 | 4 | 1,500 feet | Poor |
| Greenline | 24 | Fulton Street/OR 138E | Y | N | 4 | 4 | 0.5 miles | Poor |
| Greenline | 23 | $\begin{aligned} & \text { Ten Down Bowling, OR } \\ & \text { 138E } \end{aligned}$ | Y | Y | 4 | 4 | 1,140 feet | Fair |
| Greenline | 22 | Kowloon Restaurant, OR 138E | Y | Y | 4 | 4 | 185 feet | Fair |
| Greenline | 21 | Phoenix School, OR 138E | Y | Y | 4 | 4 | 0.6 mile | Poor |
| Greenline |  | Kincaid Drive, Les Schwab | N | N | 4 | 4 | 1.1 miles | Poor |
| Redline / Greenline | 43 | Jackson Street, Library | Y | Y | 3 | 2 | 270 feet | Good |
| Greenline | 26 | Washington Avenue and Rose Street | Y | Y | 3 | 2 | 65 feet | Good |
| Sunshine Park | 7 | Sunshine Park | Y | Y | 4 | 4 | 2.2 miles | Fair |
| Greenline | 21 | Douglas at Deer Creek Village Apts. east of Rifle Range Street | Y | Y | 3 | 4 | 400 feet | Fair |

## Safety Analysis

Methods from the ODOT Analysis Procedures Manual (APM)
${ }^{3}$, were used to identify the crash frequency, severity, type, and contributing factors at the study locations along OR 138E and parallel/connecting routes. Also, crash rates for intersections and segments were estimated and compared with appropriate Statewide average crash rates and critical crash rates. ODOT also uses the Safety Priority Index System (SPIS) ${ }^{4}$, a scoring method, to identify potential safety concerns on state highways based on frequency, fatal crashes, and crash rate in a three-year period. The state 2021 SPIS ranking was also consulted and documented.

The safety analysis is done for intersection and segments in the study area, as shown in Figure 4. The study intersections are listed in Table 5.

Figure 4 Study Intersections


[^1]Table 5: List of Study Intersections

| Intersection <br> ID | Intersection | Traffic Control |
| :---: | :--- | :--- |
| $\mathbf{1}$ | NE Stephens St./NE Winchester St. | Unsignalized |
| $\mathbf{2}$ | OR 138E/SE Stephens St. | Signalized |
| $\mathbf{3}$ | OR 138E/NE Jackson St./NE Winchester St. | Signalized |
| $\mathbf{4}$ | OR 138E/NE Fowler St | Unsignalized |
| $\mathbf{5}$ | OR 138E/NE Fulton St. | Unsignalized |
| $\mathbf{6}$ | OR 138E/NE Rifle Range St. | Signalized |
| $\mathbf{7}$ | OR 138E/NE Douglas Ave. | Unsignalized |
| $\mathbf{8}$ | SE Stephens St./SE Douglas Ave | Signalized |
| $\mathbf{9}$ | SE Douglas Ave./SE Jackson St. | Unsignalized |
| $\mathbf{1 0}$ | SE Douglas Ave./SE Kane St. | Unsignalized |
| $\mathbf{1 1}$ | SE Douglas Ave./SE Fowler St. | Unsignalized |
| $\mathbf{1 2}$ | SE Douglas Ave./SE Ramp Rd. | Unsignalized |
| $\mathbf{1 3}$ | NE Douglas Ave./NE Rifle Range St. | Unsignalized |

Figure 5. Study Segment Safety Assessment


The most recent five-year crash data available (2016-2020) were obtained from ODOT5. ODOT crash data is based on reportable motor vehicle traffic crashes. According to ODOT's 2018 Motor Vehicle Traffic Crash Analysis and Code Manual6 legally reportable motor vehicle traffic crashes involve a fatality, injury, or damage to personal property or any vehicle in excess of $\$ 2,500$. The following sections provide summaries of the intersection and segment safety analysis.

## Intersection Crashes

For this analysis, intersection-related crashes are defined as crashes that occurred within 250 feet of the intersection.

## Crash Frequency and Severity

Table 6 presents the crash frequency and severity at the study intersections for the five-year analysis period (2016-2020). Based on the five most recent years of reported crash data, no fatalities and two serious injury crashes at the study intersections (one on OR 138E at NE Fowler Street and the other at SE Douglas Avenue at SE Jackson Street) were reported during the 5

[^2]${ }^{6} 2018$ Motor Vehicle Traffic Crash Analysis and Code Manual
most recent years of reported crashes. The crash at the SE Douglas Avenue/SE Jackson Street intersection involved a pedestrian. Based on the 2021 SPIS Report7, the intersection of OR 138E/NE Pomona Street is one of the top $10 \%$ SPIS site in the state.. Appendix A shows location of crashes by severity.

Table 6: Summary of Five-Year (2016-2020) Crash Frequency by Severity at Study Intersections

| Intersections |  | Crash Severity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fatal (K) | Serious Injury (A) | Minor Injury (B) | Possible Injury (C) | Property Damage Only (O) | Total |
| 1 | NE Stephens St./NE Winchester St. | 0 | 0 | 3 | 1 | 2 | 6 |
| 2 | OR 138E/SE Stephens St. | 0 | 0 | 3 | 10 | 12 | 25 |
| 3 | OR 138E/NE Jackson St./NE Winchester St. | 0 | 0 | 3 | 4 | 4 | 11 |
| 4 | OR 138E/NE Fowler St. | 0 | 0 | 1 | 1 | 5 | 7 |
| 5 | OR 138E/NE Fulton St. | 0 | 1 | 1 | 1 | 0 | 3 |
| 6 | OR 138E/NE Rifle Range St. | 0 | 0 | 1 | 4 | 3 | 8 |
| 7 | OR 138E/NE Douglas Ave. | 0 | 0 | 1 | 0 | 0 | 1 |
| 8 | SE Stephens St./SE Douglas Ave | 0 | 0 | 4 | 10 | 8 | 22 |
| 9 | SE Douglas Ave./SE Jackson St. | 0 | 1 | 0 | 1 | 4 | 6 |
| 10 | SE Douglas Ave./SE Kane St. | 0 | 0 | 0 | 1 | 0 | 1 |
| 11 | SE Douglas Ave./SE Fowler St. | 0 | 0 | 0 | 1 | 2 | 3 |
| 12 | SE Douglas Ave./SE Ramp Rd. | 0 | 0 | 0 | 1 | 1 | 2 |
| 13 | NE Douglas Ave./NE Rifle Range St. | 0 | 0 | 1 | 0 | 0 | 1 |
| Total |  | 0 | 2 | 18 | 35 | 41 | 96 |

As shown in Table 6:

- At the OR 138E/SE Stephens Street signalized intersection - the highest number of reported crashes ( 25 crashes) were observed. $92 \%$ of the crashes (23) occurred on the SB approach of SE Stephens Street.
- SE Stephens Street/SE Douglas Avenue signalized intersection had the second highest number of crashes (22 crashes).
- OR 138E/NE Douglas Avenue (unsignalized), SE Douglas Avenue/SE Kane Street (unsignalized), and NE Douglas Avenue/NE Rifle Range Street (unsignalized) - had the lowest number of reported crashes (one each).

[^3]- OR 138E/NE Fulton Street and SE Douglas Avenue/SE Jackson Street - had the most serious injury crashes, one on each of these intersections, which are both unsignalized. The seriously injured road-user at SE Douglas Avenue/SE Jackson Street was a pedestrian and the crash involved a vehicle not yielding to the pedestrian. The lighting condition was reported dark with no streetlights which may have contributed to the driver not yielding to the pedestrian. The serious injury crash at OR 138E/NE Fulton Street was a turning movement related crash where one of the vehicles did not yield right of way and attempted to make improper left-turn movement.


## Collision Type

Table 7 presents the crash frequency by collision type at the study intersections. Overall, turning movement and rear end crashes are the most frequent collision type.

Table 7: Summary of Five-Year (2016-2020) Crash Frequency by Collision Type at Study Intersections

| Intersections |  | Collision Type |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | RearEnd | Fixed Object or Other Object | Turn | Ped | Head On | Sideswipe Overtaking | Angle | Other | Total |
| 1 | NE Stephens St./ NE Winchester St. | 1 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 6 |
| 2 | OR 138E/ <br> SE Stephens St. | 14 | 2 | 8 | 0 | 0 | 1 | 0 | 0 | 25 |
| 3 | OR 138E/ <br> NE Jackson St./ <br> NE Winchester St. | 3 | 0 | 3 | 1 | 0 | 1 | 3 | 0 | 11 |
| 4 | OR 138E/ NE Fowler St. | 1 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 7 |
| 5 | OR 138E/ <br> NE Fulton St. | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| 6 | OR 138E/ NE Rifle Range St . | 1 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 8 |
| 7 | OR 138E/ NE Douglas Ave. | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8 | SE Stephens St./ SE Douglas Ave. | 8 | 1 | 5 | 1 | 0 | 0 | 7 | 0 | 22 |
| 9 | SE Douglas Ave./ SE Jackson St. | 1 | 0 | 2 | 1 | 0 | 0 | 2* | 0 | 6 |
| 10 | SE Douglas Ave./ SE Kane St. | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11 | SE Douglas Ave./ SE Fowler St. | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 3 |
| 12 | SE Douglas Ave./ SE Ramp Rd. | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 13 | NE Douglas Ave./ NE Rifle Range St. | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total |  | 31 | 8 | 37 | 4 | 1 | 2 | 12 | 1 | 96 |

[^4]In summary:

- At OR 138E/SE Stephens Street signalized intersection - 14 out of the 25 crashes reported were rear-end crashes, and eight were turning movement crashes.
- At SE Stephens Street/SE Douglas Avenue signalized intersection - $91 \%$ of the crashes (20) occurred on SE Stephens Street approaches. Out of the 22 crashes occurring at SE Stephens Street/SE Douglas Avenue, eight of these crashes are rear-end crashes, seven of the crashes are angle, and five are turning movement related.
- At the unsignalized intersections on Diamond Lake Blvd - majority of the crashes were turning movement crashes, likely to be contributed by the uncontrolled left turn movements. Turning movement crashes are common crash type at uncontrolled intersections as drivers are burdened with the task of identifying gaps in traffic and safely crossing.
- There have been four crashes involving pedestrians; and two of these crashes resulted in minor injury of the pedestrians (at OR 138E/NE Fowler Street and OR 138E/NE Jackson Street/NE Winchester Street), one resulted in serious injury of the pedestrian (at SE Douglas Avenue/SE Jackson Street), and one in possible injury of the pedestrian (at SE Stephens Street/SE Douglas Avenue).
- At NE Douglas Avenue/NE Jackson St. there was also a crash involving a motorist disregarding a stop sign and hitting a bicyclist which resulted in possible injury of the bicyclist.


## Contributing Factors

Table 8 presents the crash frequency by contributing factor. The most frequent contributing factors were "Did not yield right-of-way", "Failed to avoid vehicle ahead", and "Followed too closely". In summary:

- Majority of the crashes at the signalized intersections OR 138E/SE Stephens Street and SE Stephens Street/SE Douglas Avenue are reportedly contributed by driving behavior, particularly the causes reported are failed to avoid vehicle ahead ( $32 \%$ ), did not yield right-of-way (23\%), disregarded traffic signal (19\%), and followed too closely (15\%). The reasons for these crashes could be attributed to either drivers not expecting to stop at the signalized intersections or making risky turning movements at the same time when there are opposing through vehicles entering the intersection.
- Three of the pedestrian crashes were contributed by the factor "did not yield" to pedestrians at the intersections of SE Stephens Street/SE Douglas Avenue(signalized), SE Douglas Avenue/SE Jackson Street (unsignalized), and OR 138E/NE Jackson Street/NE Winchester Street (signalized).

Table 8: Summary of Five-Year (2016-2020) Crash Frequency by Crash Contributing Factors at Study Intersections

|  | Intersections | Contributing Factor |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Failed to avoid vehicle ahead | $\begin{aligned} & \text { Followed } \\ & \text { too } \\ & \text { cosely } \end{aligned}$ | Disregarded trafic signal | Careless Driving | $\begin{gathered} \text { Too fost } \\ \text { for } \\ \text { condifions } \end{gathered}$ | Did not yield right-ofway | $\begin{aligned} & \text { Made } \\ & \text { improper } \\ & \text { turn } \end{aligned}$ | Other | Total |
| 1 | NE Stephens St./ NE Winchester St. | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 1 | 6 |
| 2 | OR 138E/ SE Stephens St. | 8 | 6 | 2 | 0 | 2 | 6 | 0 | 1 | 25 |
| 3 | OR 138E/ <br> NE Jackson St. / <br> NE Winchester St. | 1 | 2 | 4 | 0 | 0 | 2 | 1 | 1 | 11 |
| 4 | OR 138E/ NE Fowler St. | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 2 | 7 |
| 5 | OR 138E/ NE Fulton St. | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 3 |
| 6 | OR 138E/ NE Rifle Range St. | 0 | 1 | 0 | 0 | 0 | 6 | 0 | 1 | 8 |
| 7 | OR 138E/ NE Douglas Ave. | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 8 | SE Stephens St./ SE Douglas Ave | 7 | 1 | 7 | 0 | 1 | 5 | 0 | 1 | 22 |
| 9 | SE Douglas Ave./ SE Jackson St. | 1 | 0 | 1 | 0 | 0 | 2 | 1 | 1 | 6 |
| 10 | SE Douglas Ave./ SE Kane St. | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 11 | SE Douglas Ave./ SE Fowler St. | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 3 |
| 12 | SE Douglas Ave./ SE Ramp Rd. | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 |
| 13 | NE Douglas Ave./ NE Rifle Range St. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| Total |  | 18 | 13 | 14 | 2 | 3 | 29 | 7 | 10 | 96 |

## Crash Rates

The crash rates for each intersection were calculated based on the total entering average annual daily traffic (AADT) at the intersection. For example, the AADT of OR 138E is on average $15,600 \mathrm{vpd}$, estimated from the 2023 balanced peak hour volumes (PHV) with the assumption that the PHV is $10 \%$ of the AADT.

Critical crash rate was calculated for each intersection using the procedure provided in ODOT APM. According to the APM, there needs to be at least five to ten sites in each reference population for this method to be statistically valid. Therefore, to have enough candidates for a reference population the intersections were grouped into signalized (four in total) and unsignalized (nine in total) intersections. Statewide $90^{\text {th }}$ percentile crash rates were obtained using comparable intersection referenced from the ODOT APM, Exhibit 4-11. Observed crash rates were compared to critical crash rate and the statewide $90^{\text {th }}$ percentile crash rate. Table 9 presents the comparison of crash rates with the statewide $90^{\text {th }}$ percentile crash rates and the critical crash rate.

From the comparative analysis of crash rates, it was found that:

- Signalized OR 138E/SE Stephens Street - exceeded the Statewide Crash Rate
- Unsignalized SE Douglas Avenue/SE Jackson Street - observed crash rate was higher than both Critical Crash Rate and the Statewide Crash Rate.
- Unsignalized SE Douglas Avenue/SE Fowler Street - exceeded the Statewide Crash Rate

Table 9: Comparison of Crash Rates per Million Entering Vehicles (MEV) with Statewide Crash Rate ${ }^{8}$ and Critical Crash Rate

| Intersections |  | Intersection Type | Control Type | Observed Crash Rate | Critical Crash Rate | Statewide 90h <br> Percentile <br> Crash Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | NE Stephens St./ NE Winchester St. | 3ST | Unsignalized | 0.13 | 0.26 | 0.29 |
| 2 | OR 138E/ SE Stephens St. | 3SG | Signalized | 0.56 | Not enough sites | 0.51 |
| 3 | OR 138E/ NE Jackson St. / NE Winchester St. | 4SG | Signalized | 0.27 | Not enough sites | 0.86 |
| 4 | OR 138E/ NE Fowler St. | 3ST | Unsignalized | 0.18 | 0.27 | 0.29 |
| 5 | OR 138E/ NE Fulton St. | 4ST | Unsignalized | 0.09 | 0.28 | 0.41 |
| 6 | OR 138E/ NE Rifle Range St. | 4SG | Signalized | 0.26 | Not enough sites | 0.86 |
| 7 | OR 138E/ NE Douglas Ave. | 3ST | Unsignalized | 0.05 | 0.32 | 0.29 |
| 8 | SE Stephens St./ SE Douglas Ave | 4SG | Signalized | 0.50 | Not enough sites | 0.86 |
| 9 | SE Douglas Ave./ SE Jackson St. | 4ST | Unsignalized | 0.45 | 0.37 | 0.41 |
| 10 | SE Douglas Ave./ SE Kane St. | 3ST | Unsignalized | 0.09 | 0.39 | 0.29 |
| 11 | SE Douglas Ave./ SE Fowler St. | 3ST | Unsignalized | 0.30 | 0.42 | 0.29 |
| 12 | SE Douglas Ave./ SE Ramp Rd. | 3ST | Unsignalized | 0.25 | 0.45 | 0.29 |
| 13 | NE Douglas Ave./ NE Rifle Range St. | 3ST | Unsignalized | 0.19 | 0.54 | 0.29 |

3SG three-leg signalized; 3ST: three-leg minor stop-control; 4SG: four-leg signalized; 4ST: four-leg minor stop-control
Red- indicates crash rates that exceed Statewide crash rates or critical crash rate

## Segment Crashes

This section summarizes the crashes that occurred on OR 138E, SE Stephens Street, and Douglas Avenue from SE Stephens Street in the west to the Urban Growth Boundary in the east. The analysis focuses on crashes on the roadway segments as shown in Figure 5; crashes at the study intersections were excluded from these study segments.

[^5]
## Crash Frequency and Severity

Table 10 presents the five-year crash summary by frequency and severity at the study segments. To summarize:

- OR 138E between NE Rifle Range Street and NE Douglas Avenue - the highest frequency of crashes occurred on this segment, with two of them resulting in fatal crashes and two in serious-injury crashes.
- OR 138E between NE Fowler Street and NE Rifle Range Street - this segment had the second highest frequency of crashes, with one of the fatal crashes occurring on this segment. Majority of the crashes on this segment are property damage only.
- OR 138E between NE Douglas Avenue to East - this segment had a high crash frequency (11) but none of them resulted in fatal or serious injury crash.
- NE Winchester Street/NE/SE Jackson Street - there were ten injury crashes on this segment with one of them being a serious injury crash. There were two crashes involving a bicyclist and a motorist resulting in a minor injury and possible injury of the bicyclists.
- SE Douglas Avenue between SE Fowler Street and NE Rifle Range Street - another segment with a high crash frequency (ten) and a serious injury crash (one). The serious injury crash resulted from a motorist hitting a bicyclist while the motorist was reportedly making an improper turning movement. Another crash involving a bicyclist and a motorist was observed on this segment which resulted in minor injury of the bicyclist.

Table 10: Summary of Five-Year (2016-2020) Crash Frequency by Severity at Study Segments

| Segment | Crash Severity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fatal (K) | Serious Injury (A) | Minor Injury (B) | Possible Injury (C) | Property Damage Only (O) | Tołal |
| A. OR 138E <br> (SE Stephens St. to NE Fowler St.) | 0 | 0 | 0 | 0 | 0 | 0 |
| B. OR 138E <br> (NE Fowler St. to NE Rifle Range St.) | 1 | 0 | 4 | 3 | 11 | 19 |
| C. OR 138E <br> (NE Rifle Range St. to NE Douglas Ave.) | 2 | 2 | 5 | 5 | 10 | 24 |
| $\begin{aligned} & \text { D. OR 138E } \\ & \text { (NE Douglas Ave. to East study area) } \end{aligned}$ | 0 | 0 | 3 | 2 | 6 | 11 |
| E. SE Douglas Ave. (SE Stephens St. to SE Fowler St.) | 0 | 0 | 0 | 0 | 0 | 0 |
| F. SE Douglas Ave. (SE Fowler St. to NE Rifle Range St.) | 0 | 1 | 1 | 1 | 7 | 10 |
| G. NE Douglas Ave. (NE Rifle Range St. to OR 138E) | 0 | 0 | 1 | 0 | 1 | 2 |
| H. SE Stephens St. (NE Winchester St. to SE Douglas Ave.) | 0 | 0 | 0 | 3 | 2 | 5 |
| I. NE Winchester St./NE Jackson St./SE Jackson St. | 0 | 1 | 3 | 6 | 8 | 18 |
| Total | 3 | 4 | 17 | 20 | 45 | 89 |

## Crash by Collision Type

Table 11 summarizes the segment crashes by collision types. Most frequent collision type reported was the turning movement crashes, followed by rear-end. There were no pedestrian crashes reported on these segments.

In summary:

- OR 138E (NE Rifle Range Street to NE Douglas Avenue) - one of the fatal crashes on the segment resulted from a head-on collision and another one from two vehicles colliding at an angle at the intersection of OR 138E/Kincaid Drive. The two serious injury crashes involved left turning movements at the same intersection where drivers apparently did not yield right of way.
- OR 138E (NE Fowler Street to the East study boundary) - majority of the crashes were turning movement crashes, with a high number of fixed object crashes and crashes which were reported as miscellaneous. Miscellaneous collisions include for example hitting a wild or domestic animal, lost load, or drive shaft fell from vehicle.
- SE Douglas Avenue (SE Fowler Street to NE Rifle Range Street) - collision types that were observed included three backing crashes, two rear-end and sideswipe crashes, and one turning movement, one angle, and one miscellaneous. The turning movement and angle crashes involved a motorist hitting a bicyclist.
- NE Winchester Street/NE/SE Jackson Street - majority of the crashes were rear-end and turning movement related. There were two crashes involving bicycles hit by motorists which were turning or collide in a straight angle.

Table 11: Summary of Five-Year (2016-2020) Crash Frequency by Collision Type at Study Segments

| Segment | Collision Type |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rear -End | Turn | Fixed Object or Other Object | HeadOn | Angle | Sideswipe | Backing | Misc. | Other | Total |
| A. OR 138E <br> (SE Stephens St. to NE Fowler St.) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B. OR 138E (NE Fowler St. to NE Rifle Range St.) | 1 | 15 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 19 |
| C. OR 138E (NE Rifle Range St. to NE Douglas Ave) | 3 | 11 | 5 | 1 | 1 | 1 | 0 | 2 | 0 | 24 |
| D. OR 138E (NE Douglas Ave. to East) | 1 | 3 | 1 | 0 | 0 | 2 | 0 | 3 | 1 | 11 |
| E. SE Douglas Ave. (SE Stephens St. to SE Fowler St.) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| F. SE Douglas Ave. (SE Fowler St. to NE Rifle Range St.) | 2 | 1* | 0 | 0 | 1* | 2 | 3 | 1 | 0 | 10 |
| G. NE Douglas Ave (NE Rifle Range St. to OR 138E) | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |


| H. SE Stephens St. (NE <br> Winchester St. to SE <br> Douglas Ave.) | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I. NE Winchester St/ <br> NE Jackson St./ <br> SE Jackson St. | 7 | $8^{*}$ | 1 | 0 | $2^{*}$ | 0 | 0 | 0 | 0 | 18 |
| Total | 16 | 42 | 11 | 1 | 4 | 5 | 3 | 6 | 1 | 89 |

Note:

* Indicates one of these crashes involved a bicyclist.


## Contributing Factors

Table 12 presents the distribution of crashes by crash contributing factors on the study segments. Similar to the intersection crash trends, "Did not yield right-of-way" and "Followed too closely" were the major contributing factors of crashes on OR 138E The "Other" category included improper driving actions such as improper turn, improper change of lanes, inattention, etc.

Table 12: Summary of Five-Year (2016-2020) Crash Frequency by Crash Cause (by Segments)

| Segment | Contributing Factor |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Did not yield right-ofway | Followed too closely | Made improper furn | Inattention | Careless Driving | Failed to avoid vehicle ahead | Other | Total |
| A. OR 138E <br> (SE Stephens St. to NE Fowler St.) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B. OR 138E (NE Fowler St. to NE Rifle Range) | 11 | 1 | 4 | 0 | 0 | 0 | 3 | 19 |
| C. OR 138E (NE Rifle Range St. to NE Douglas Ave.) | 11 | 1 | 0 | 1 | 0 | 1 | 10 | 24 |
| D. OR 138E (NE Douglas Ave. to East) | 2 | 0 | 1 | 2 | 0 | 0 | 6 | 11 |
| E. SE Douglas Ave. (SE Stephens St. to SE Fowler St.) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| F. SE Douglas Ave. (SE Fowler St. to NE Rifle Range St.) | 2 | 1 | 0 | 2 | 0 | 0 | 5 | 10 |
| G. NE Douglas Ave. (NE Rifle Range St. to OR 138E) | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| H. SE Stephens St. (NE Winchester St. to SE Douglas Ave.) | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 5 |
| I. NE Winchester St./NE Jackson St./SE Jackson St. | 6 | 6 | 2 | 1 | 0 | 1 | 2 | 18 |
| Total | 35 | 11 | 8 | 6 | 0 | 2 | 27 | 89 |

## Crash Rates

The crash rates for the OR 138E arterial segments and the collector roads connecting to the OR 138E were computed using the observed crashes (2016-2020) and the AADT estimated using 2023 turning movement data. The statewide average crash rates for "Other Principal Arterials" and "Urban Collectors" were computed using the Table II: Five-Year Comparison of State Highway Crash Rates", which provided statewide crash rates for the facilities between 2016 and 2020. Segment critical crash rates were also calculated using the Critical Rate Calculator ${ }^{10}$ provided in the APM ${ }^{11}$. The segments were categorized as arterials and collectors. Since there were less than five sites in the collector category, no critical crash rate was calculated for collector roads in the corridor. The findings from the analysis in Table 13 are summarized below:

- OR 138E (NE Fowler Street to NE Rifle Range Street), and (NE Rifle Range Street to NE Douglas Avenue) - observed crash rates exceed the calculated critical crash rates for arterials.
- NE Winchester Street/NE/SE Jackson Street - observed crash rate was higher than the Statewide Average Crash Rate for Collector roads.

Table 13: Comparison of Crash Rates with the Statewide Crash Rates for Segments

| Segment | Segment <br> Type | Observed <br> Crash Rate | Critical <br> Crash Rate | Statewide <br> Average <br> Crash Rate |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
| A. | OR 138E (SE Stephens St. to NE Fowler St.) | Arterial | 0.00 | 2.68 | 0.55 |
| B. | OR 138E (NE Fowler St. to NE Rifle Range St.) | Arterial | 0.80 | 2.68 | 0.55 |
| C. | OR 138E (NE Rifle Range St. to NE Douglas <br> Ave.) | Arterial | 0.64 | 2.68 | 0.55 |
| D. | OR 138E (NE Douglas Ave. to East) | Arterial | 0.34 | 2.68 | 0.55 |
| E. | SE Douglas Ave. (SE Stephens St. to SE <br> Fowler St.) | Collector | 0.00 | 2.02 | Not enough <br> sites |
| F. | SE Douglas Ave. (SE Fowler St. to NE Rifle <br> Range St.) | Collector | 1.98 | 2.02 | Not enough <br> sites |
| G. | NE Douglas Ave. (NE Rifle Range St. to OR <br> 138E) | Collector | 0.30 | 2.02 | Not enough <br> sites |
| H. | SE Stephens St. (NE Winchester St. to SE <br> Douglas Ave.) | Arterial | 0.36 | 2.68 | 0.55 |
| I. | NE Winchester St./NE Jackson St/SE Jackson <br> St. | Collector | 2.12 | 2.02 | Not enough <br> sites |

Red- indicates crash rates that exceed Statewide Crash Rates or Critical Crash Rates.

## Crash Trends and Potential Countermeasures

This section summarizes crash trends identified in the crash analysis and potential countermeasures. Countermeasures are often implemented as strategies intended to reduce crash frequency or severity on the road for all users. The Oregon Department of Transportation, under the All Roads Transportation Safety (ARTS) Program, provides safety practitioners with a list of effective countermeasures that are appropriate improvements to many common safety issues. Each countermeasure is associated with a Crash Reduction Factor (CRFs). CRFs indicate

[^6]the effectiveness of a countermeasure by providing the change (reduction) in crash frequency after the implementation of the countermeasure. Following are crash trends identified from the analysis and potential countermeasures shown in Table 14:

## OR 138E/SE Stephens St. and SE Stephens St./SE Douglas Ave (signalized)

- Highest observed crash frequencies.
- Majority of these crashes are rear-end crashes and turning movement crashes on the SB approach of the intersections.
- Contributed mostly by improper driving behavior.
- One pedestrian crash at SE Stephens Street/SE Douglas Avenue resulting in possible injury of the pedestrian.
- Observed crash rate at OR 138E/SE Stephens Street exceeded the Statewide Crash Rate


## OR 138E/NE Jackson St./NE Winchester St. (signalized)

- A pedestrian crash possibly contributed by motorist not yielding right of way resulting in minor injury.


## Unsignalized intersections

- Majority of the crashes are turning movement crashes, likely to be contributed by the uncontrolled left turn movements.
- Two of the pedestrian crashes at unsignalized intersections (OR 138E/NE Fowler Street and SE Douglas Avenue/SE Jackson Street) resulted in injuries of the pedestrians.
- At SE Douglas Avenue/SE Jackson Street, a pedestrian crash reportedly occurred in darkness with no streetlights.
- At SE Douglas Avenue/SE Jackson Street, a bicyclist sustained possible injury when hit by a motorist disregarding a stop sign.
- Observed crash rate at SE Douglas Avenue/SE Jackson Street exceeded both critical crash rate and Statewide Crash Rate.


## Segments on OR 138E

- Highest frequency of crashes between NE Fowler Street and NE Douglas Avenue with three fatal injury crashes and two serious injury crashes with the majority of these crashes occurring at the intersection of OR 138E/Kincaid Drive.
- The two segments on OR 138 between NE Fowler Street and NE Douglas Avenue exceed the calculated critical crash rates for arterials.


## Segments on Douglas Avenue

- Three backing crashes occurred on segments of Douglas Avenue which are two-way one-lane in each direction with on-street parking observed on Google Streetview.
- There were two bicycle crashes at or near the unsignalized intersections of Douglas Avenue. It must be mentioned that Douglas Avenue does not have a dedicated bike lane.


## Segments on NE Winchester Street/NE Jackson Street/SE Jackson Street

- None of the intersections of NE Winchester Street with the local streets are signalized. Majority of the crashes observed are rear-end and turning movement.
- Seven of these rear-end/turning movement crashes are at the non-study intersection of NE Winchester Street/NE Wright Avenue
- There were two bicyclists involved crashes with injuries sustained by the bicyclists. The crashes were of turning movement and angle collision type.
- Observed crash rate exceeded the Statewide Average Crash Rate.

Based on the summary provided above, it appears that the following intersections and segments need to be the focus of further safety assessment and potential countermeasures should be identified:

1. Intersection 2: OR 138E/SE Stephens Street
2. Intersection 8: SE Stephens Street/SE Douglas Avenue
3. Intersection 3: OR 138E/NE Jackson Street/NE Winchester Street
4. Intersection 4: OR 138E/NE Fowler Street
5. Intersection 9: SE Douglas Avenue/SE Jackson Street
6. Segment B: OR 138E between NE Fowler Street and NE Rifle Range Street
7. Segment C: OR 138E between NE Rifle Range Street and NE Douglas Avenue
8. Segment F: SE Douglas Avenue between SE Fowler Street and NE Rifle Range Street
9. Segment I: NE Winchester Street/NE Jackson Street/SE Jackson Street

Table 14: Potential Countermeasures

| Target crashes | Location | Potential Countermeasures |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | \# | Description | CRF | Target Crash |
| Left turning movement crashes | Signalized OR 138E/ SE Stephens St. <br> Signalized SE Stephens St./ SE Douglas Ave. | 19 | Replace Urban Permissive or Protected/Permissive Left Turns to Protected Only | 99 | Left Turning Crashes at All Severities |
|  |  | 113 | Install Coordination or Adaptive Signal Timing of Urban Traffic Signals | 17 | All Crashes at All Severities |
|  |  | 116 | Install Actuated/Coordinated Flashing Beacons as Advance Warning for Signalized Intersections | 36 | Rear End Crashes at All Severities |
| Pedestrian and Bicycle crashes | Signalized <br> OR 138E/ <br> NE Jackson St./ <br> NE Winchester St. <br> Signalized <br> OR 138E/ <br> NE Jackson St./ <br> NE Winchester St. <br> Signalized SE Stephens St./SE Douglas Ave. | BP1 | Install Pedestrian Countdown Timer(s) | 70 | Pedestrian Crashes at All Severities |
|  |  | BP3 | Install Urban Leading <br> Pedestrian or Bicycle Interval at Signalized Intersections | 37 | Pedestrian and Bicycle Crashes at All Severities |
| Pedestrian and Bicycle crashes | Unsignalized <br> OR 138E/ <br> NE Fowler St. <br> Unsignalized SE Douglas Ave./SE Jackson St. | BP2 | Provide Intersection Illumination (Bike \& Ped) | 42 | Nighttime Pedestrian and Bicycle Crashes at All Injury Severities |
|  |  | BP11 | Install Rectangular Rapid Flashing Beacon with Median (3-Lane or More Roadway) | 56 | Pedestrian Crashes at All Severities |
| Bicycle crashes | SE Douglas Ave. | BP22 | Install Bike Lanes | 36 | Bicycle crashes at all severities |
| Bicycle crashes | SE Douglas Ave/ OR 138E | BP23 | Install Cycle Tracks | 59 | Bicycle crashes at all severities |
| Bicycle Crashes | Segment NE Winchester St./ NE Jackson St./ SE Jackson St. | BP6 | Install Urban Green Bike Lanes at Conflict Points | 39 | Bicycle Crashes at All Severities |
| Turning movement crashes | NE Winchester St./ <br> NE Jackson St./ SE Jackson St. <br> OR 138E (NE Fowler St. to NE Rifle Range St.) | H18 | Install Roundabout from Minor Road Stop Control | 82 | All crashes at all Injury severities |
|  |  | $\begin{aligned} & \mathrm{H} 22 \\ & \mathrm{H} 23 \end{aligned}$ | Install Urban Traffic Signal | 67 angle <br> -143 rear end | Angle \& Rear End Crashes at All Severities |
| \#- ODOT Countermeasure Number; CRF - ODOT Crash Reduction Factor |  |  |  |  |  |

## Existing Traffic Conditions

This section summarizes the existing traffic conditions on the OR 138E study corridor and supporting local street network. The information in this section will provide a basis for comparison with future growth projections and will inform the identification of various multimodal improvement opportunities.

## Current Transportation System Operations

Existing PM peak hour traffic operations were analyzed for the study intersections shown in Figure 6 and summarized in Table 15. The traffic operations analysis was completed in accordance with the methodology outlined in Technical Memorandum \#1 (Methodology Memorandum), which is based on the guidance in the APM.

Figure 6. Study Intersections


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\& ASSOCIATES
Study Intersections

Table 15: Study Intersections

| Map <br> ID | Intersection | Count Dates | Count Type |
| :--- | :--- | :--- | :--- |
| 1. | NE Stephens St./NE Winchester St. | $04 / 06 / 2022$ | 16 hour |
| 2. | OR 138E/SE Stephens St. | $03 / 28 / 2022$ | 16 hour |
| 3. | OR 138E/NE Jackson St./NE Winchester St. | $03 / 28 / 2022$ | 16 hour |
| 4. | OR 138E/NE Fowler St. | $03 / 28 / 2022$ | 4 hour |
| 5. | OR 138E/NE Fulton St. | $03 / 28 / 2022$ | 16 hour |
| 6. | OR 138E/NE Rifle Range St. | $03 / 28 / 2022$ | 16 hour |
| 7. | OR 138E/NE Douglas Ave. | $03 / 28 / 2022$ | 4 hour |
| 8. | SE Stephens St./SE Douglas Ave. | $03 / 30 / 2022$ | 16 hour |
| 9. | SE Douglas Ave./NE Jackson St. | $03 / 30 / 2022$ | 4 hour |
| 10. | SE Douglas Ave./SE Kane St. | $03 / 30 / 2022$ | 4 hour |
| 11. | SE Douglas Ave./NE Fowler St. | $03 / 30 / 2022$ | 4 hour |
| 12. | SE Douglas Ave./SE Ramp Rd. | $03 / 30 / 2022$ | 4 hour |
| 13. | NE Douglas Ave./NE Rifle Range St. | $03 / 30 / 2022$ | 4 hour |

## Traffic Counts

Manual vehicle turning movement, pedestrian, bicycle, and heavy vehicle counts were conducted at the study intersections between March 28th and April $6^{\text {th }} 2022$. The counts were conducted by ODOT on a typical mid-weekday and consists of 16 -hour and 4-hour counts as outlined in Table 15. The counts include the total number of pedestrians, bicyclists, and motor vehicles that entered the study intersections in 15-minute intervals. The traffic count worksheets are provided in Attachment B.

## Peak Hour Development

The traffic counts were reviewed to determine individual and system-wide peak hours for the operational analyses. A system-wide peak hour approach was determined to be most appropriate based on the data. Two system-wide peak hours were identified for the study intersections. A 4:00 to 5:00 PM peak hour was identified along OR 138E and SE Stephens Street and a 2:00 to 3:00 PM peak hour was identified along SE Douglas Avenue between SE Jackson Street and NE Rifle Range Street.

## Intersection Operational Standards

ODOT uses volume-to-capacity (V/C) ratios to assess intersection operations. Table 6 of the Oregon Highway Plan (OHP) and Table 1200-1 of the Oregon Highway Design Manual (HDM) provide maximum volume-to-capacity ratios for all signalized and unsignalized intersections located outside the Portland metropolitan area.

The OHP volume to capacity ratios are used to evaluate existing and future no-build conditions, while the HDM ratios are used in the creation of design concept plan alternatives including projects along state highways. ODOT controls all intersections along OR 138E and Stephens Street within the project area except for NE Stephens St./NE Winchester St. which is controlled by the City of Roseburg. Table 16 summarizes the v/c ratios that will be used to identify the existing and potential future operational issues at the ODOT study intersections.

Table 16: ODOT Mobility Targets/Standards

| $\begin{gathered} \text { Map } \\ \text { ID } \end{gathered}$ | Intersection | Traffic Control | OHP Mobility Target | HDM Standard |
| :---: | :---: | :---: | :---: | :---: |
| 2 | OR 138E/ <br> SE Stephens St. | Signal | 0.90 | 0.75 |
| 3 | OR 138E/ <br> NE Jackson St./ NE Winchester St. | Signal | 0.90 | 0.75 |
| 4 | OR 138E/ NE Fowler St. | TWSC ${ }^{1}$ | 0.90 major approach/ 0.95 minor approach | 0.75 |
| 5 | OR 138E/ NE Fulton St. | TWSC ${ }^{1}$ | 0.90 major approach/ 0.95 minor approach | 0.75 |
| 6 | OR 138E/ NE Rifle Range St. | Signal | 0.90 | 0.75 |
| 7 | OR 138E/ NE Douglas Ave. | TWSC ${ }^{1}$ | 0.85 major approach/ 0.90 minor approach | 0.75 |
| 8 | SE Stephens St./ SE Douglas Ave. | Signal | 0.90 | 0.75 |

As part of the 2019 Transportation System Plan update, City of Roseburg updated its mobility standards to be consistent across the City. A dual standard based on volume-to-capacity (v/c) and level of service (LOS) has been adopted. V/C and LOS are the measures to determine what is acceptable or unacceptable traffic flow on Roseburg streets. LOS is based on average seconds of delay and $v / c$ is a measure of the traffic volume/demand compared to capacity.

The City's TSP sets a maximum LOS Standard of "E" for all signalized and unsignalized intersections including County and State roadways within Roseburg city limits. Table 17 summarizes the standards that will be used to identify existing and potential future operational issues at the City study intersections. City streets shall maintain a LOS of "E" and v/c no worse than 0.95 during the peak hour of the day.

Table 17: City of Roseburg Mobility Standards

| Map ID | Intersection | Traffic Control | V/C ${ }^{1}$ | LOS ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | NE Stephens St./NE Winchester St. | TWSC3 | 0.95 | E |
| 9 | SE Douglas Ave./NE Jackson St. | AWSC4 | 0.95 | E |
| 10 | SE Douglas Ave./SE Kane St. | TWSC3 | 0.95 | E |
| 11 | SE Douglas Ave./NE Fowler St. | TWSC3 | 0.95 | E |
| 12 | SE Douglas Ave./SE Ramp Rd. | TWSC3 | 0.95 | E |
| 13 | NE Douglas Ave./NE Rifle Range St. | TWSC3 | 0.95 | E |
| 1. City intersections shall be analyzed at a peak hour factor of 1.0. <br> 2. For roadways within the city of Roseburg that are under ODOT or Douglas County jurisdiction, the mobility standards/targets of those agencies will apply. <br> 3. Two-Way Stop-Controlled (TWSC). Note the Stephens St/Winchester St intersection is a Right-in, Right-out, Left-in intersection with a yield controlled right-out, and stop-controlled right-in but for simplicity is referred to as a TWSC intersection. <br> 4. All-Way Stop-Controlled (AWSC). |  |  |  |  |

## Intersection Operations

Figure 7 shows the existing lane configurations and traffic control devices while Figure 8 summarized the PM peak hour volumes and corresponding traffic operations. As shown in Figure 8 and Table 18, all of the study intersections currently operate under the applicable ODOT mobility target and/or City operating standards. Appendix C contains the existing traffic conditions worksheets.

Table 18: Existing Traffic Conditions, Weekday PM Peak Hour

| Intersection |  | Maximum Operating Standard/Target | Weekday PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Critical Approach/Lane | LOS | Delay (sec) | V/C |
| 1 | NE Stephens St./ NE Winchester St. |  | V/C: 0.95; LOS E | WB | D | 28.2 | 0.82 |
| 2 | OR 138E/ SE Stephens St. | V/C: 0.90 | - | C | 22.3 | 0.61 |
| 3 | OR 138E/NE Jackson St./ NE Winchester St. | V/C: 0.90 | - | C | 26.0 | 0.62 |
| 4 | OR 138E/ NE Fowler St. | V/C: 0.90 major approach/ 0.95 minor approach | NB LT | F | 69.1 | 0.28 |
| 5 | OR 138E/ NE Fulton St. | V/C: 0.90 major approach/ 0.95 minor approach | NB | C | 16.7 | 0.15 |
| 6 | OR 138E/ <br> NE Rifle Range St. | V/C: 0.90 | - | A | 6.5 | 0.46 |
| 7 | OR 138E/ NE Douglas Ave. | V/C: 0.85 major approach/ 0.90 minor approach | NB | B | 11.7 | 0.03 |
| 8 | SE Stephens St./ SE Douglas Ave. | V/C: 0.90 | - | B | 14.7 | 0.62 |
| 9 | SE Douglas Ave./ NE Jackson St. | V/C: 0.95; LOS E | SB TL | C | 18.3 | 0.31 |
| 10 | SE Douglas Ave./ SE Kane St. | V/C: 0.95; LOS E | NB LT | C | 15.3 | 0.14 |
| 11 | SE Douglas Ave./ NE Fowler St. | V/C: 0.95; LOS E | SB | B | 13.7 | 0.20 |
| 12 | SE Douglas Ave./ SE Ramp Rd. | V/C: 0.95; LOS E | NB LT | B | 14.3 | 0.29 |
| 13 | NE Douglas Ave./ NE Rifle Range St. | V/C: 0.95; LOS E | SB | B | 10.2 | 0.16 |




Table 19 shows the existing 95 ${ }^{\text {th }}$ percentile queues at the key high-volumes study intersections along the OR 138E corridor. As shown, all existing queves are contained within the defined/striped turn lanes or roadway approaches. While not summarized in Table 19, field observations noted insignificant or minimal queuing issues on intersections along the NE Douglas Avenue corridor.

Table 19: Existing 95th Percentile Queues (Synchro Output)

| Intersection |  | Critical Movements | Storage (it) | 95ih Percentile Queve (fi) | Queve Storage Adequate? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | OR 138E/ SE Stephens St. | NB RT WB LT SB LT | $\begin{aligned} & 125 \\ & 375 \\ & 200 \end{aligned}$ | $\begin{gathered} 50 \\ 100 \\ 150 \end{gathered}$ | Yes Yes Yes |
| 3 | OR 138E/ NE Jackson St./ NE Winchester St. | NB LT <br> NB RT <br> WB LT <br> WB RT <br> SB LT <br> SB TH RT <br> EB LT <br> EB RT | $\begin{gathered} \hline 80 \\ 125 \\ 250 \\ 50 \\ 400 \\ 300 \\ 175 \\ 50 \end{gathered}$ | $\begin{gathered} 25 \\ 100 \\ 50 \\ 50 \\ 400 \\ 100 \\ 75 \\ 50 \end{gathered}$ | Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes |
| 4 | OR 138E/ NE Fowler St. | NB LT NB RT WB LT | $\begin{aligned} & 125 \\ & 200 \\ & 150 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \\ & 25 \end{aligned}$ | Yes Yes Yes |
| 5 | OR 138E/ <br> NE Fulton St. | WB LT EB LT | $\begin{aligned} & >200 \\ & >200 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ |
| 6 | OR 138E/ <br> NE Rifle Range St. | NB LT NB THRT WB LT WB THRT SB LT SB THRT EB LT EB TH RT | $\begin{gathered} \hline 300 \\ 300 \\ 250 \\ >500 \\ 200 \\ >200 \\ 250 \\ >500 \end{gathered}$ | $\begin{gathered} 75 \\ 25 \\ 25 \\ 100 \\ 25 \\ 25 \\ 25 \\ 124 \end{gathered}$ | Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes |
| 7 | OR 138E/ NE Douglas Ave. | NB WB LT | $\begin{gathered} \hline>300 \\ 150 \end{gathered}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | Yes Yes |
| 8 | SE Stephens St./ SE Douglas Ave. | WB LT <br> WB TH RT <br> SB LT <br> SB TH RT <br> EB LT <br> EB TH RT | $\begin{gathered} 200 \\ 200 \\ 150 \\ >500 \\ 75 \\ 200 \end{gathered}$ | $\begin{gathered} 150 \\ 100 \\ 75 \\ 250 \\ 75 \\ 50 \end{gathered}$ | Yes <br> Yes <br> Yes <br> Yes <br> Yes <br> Yes |

## Freight Analysis

Despite having a Regional Highway designation, the OR 138E study corridor is not formally classified as an Oregon Freight Route in the Oregon Highway Plan, nor is it classified as a National Highway Freight Route. It is however, classified as a Reduction Review Route. This designation protects the vertical and horizontal clearance of the highway used to accommodate motor vehicle from modification unless there is a viable safety or access consideration that would be solved by the modification.

Based on a review of historical count data available on the ODOT TransGIS website and the 2022 traffic volume counts collected as part of this project, Table 20 summarizes the percentage of heavy vehicles on key roadway segments within the study corridor.

Table 20: OR 138E Freight Summary

| Segment | \% of Heavy <br> Average Annual <br> Daily Traffic | \% of Heavy <br> Vehicles¹ from <br> ODOT TransGIS Data | Vehicles' from 2022 <br> Traffic Counts |
| :--- | :---: | :---: | :---: |
| A. OR 138E <br> (SE Stephens St. to NE Fulton St.) | $\sim 18,000$ | $8.9 \%$ | $11 \%$ |
| B. OR 138E <br> (NE Fulton St. to NE Rifle Range St.) | $\sim 16,000$ | $8.9 \%$ | $9 \%$ |
| C. OR 138E <br> (NE Rifle Range St. to NE Douglas Ave.) | $\sim 12,000$ | $8.9 \%$ | $8 \%$ |
| H. SE Stephens St. <br> (SE Douglas Ave. to OR 138E) |  |  |  |
| 'Including FHWA Class 4 through Class 13 vehicles as categorized according to the Federal Highway Administration (FHWA) vehicle <br> classifation summary. |  |  |  |

In general, heavy vehicle trips make up approximately $9 \%$ - $11 \%$ of the overall daily traffic on the OR 138E corridor with a slightly higher percentage of heavy vehicles on the west end of the corridor. Although not summarized in Table 20, traffic counts along the SE Douglas Avenue corridor were relatively minimal.

## Pedestrian and Bicycle Volumes

Appendix B includes detailed pedestrian and bicycle counts collected at each of the study intersections over the varying count durations. For a visual summary, the weekday PM peak hour pedestrian and bicycle movements at key study intersections are summarized in Table 21 below. Key findings from these counts:

- Pedestrian volumes are highest at the west end of the study area.
- NE Jackson Street and NE Rifle Range Street had the highest number of pedestrian crossings along the OR 138E corridor.
- There was minimal bicycle trips measured at the study area intersections. This is most likely a reflection of the lack of bicycle lane infrastructure in the study area.



## Appendix A Crash Data



KITTELSON
\& ASSOCIATES


## Appendix B Traffic Counts




Peak-Hour: 4:15 PM -- 5:15 PM
Peak 15-Min: 5:00 PM -- 5:15 PM


| 15-Min Count Period Beginning At | 19853 - SE Stephens St (Northbound) |  |  |  | 19853 - SE Stephens St (Southbound) |  |  |  | NE Diamond Lake Blvd (Eastbound) |  |  |  | NE Diamond Lake Blvd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 2:00 PM | 0 | 117 | 66 | 0 | 50 | 111 | 0 | 0 | 0 | 0 | 0 | 0 | 74 | 0 | 24 | 0 | 442 |  |
| 2:15 PM | 0 | 114 | 86 | 0 | 52 | 142 | 0 | 0 | 0 | 0 | 0 | 0 | 97 | 0 | 30 | 0 | 521 |  |
| 2:30 PM | 0 | 133 | 59 | 0 | 52 | 136 | 0 | 0 | 0 | 0 | 0 | 0 | 82 | 0 | 28 | 0 | 490 |  |
| 2:45 PM | 0 | 136 | 98 | 0 | 50 | 142 | 0 | 0 | 0 | 0 | 0 | 0 | 83 | 0 | 17 | 0 | 526 | 1979 |
| 3:00 PM | 0 | 152 | 76 | 0 | 44 | 138 | 0 | 0 | 0 | 0 | 0 | 0 | 104 | 0 | 25 | 0 | 539 | 2076 |
| 3:15 PM | 0 | 127 | 73 | 0 | 53 | 132 | 0 | 0 | 0 | 0 | 0 | 0 | 115 | 0 | 46 | 0 | 546 | 2101 |
| 3:30 PM | 0 | 128 | 95 | 0 | 57 | 119 | 0 | 0 | 0 | 0 | 0 | 0 | 97 | 0 | 34 | 0 | 530 | 2141 |
| 3:45 PM | 0 | 141 | 99 | 0 | 54 | 126 | 0 | 0 | 0 | 0 | 0 | 0 | 123 | 0 | 36 | 0 | 579 | 2194 |
| 4:00 PM | 0 | 135 | 82 | 0 | 54 | 139 | 0 | 0 | 0 | 0 | 0 | 0 | 92 | 0 | 26 | 0 | 528 | 2183 |
| 4:15 PM | 0 | 130 | 83 | 0 | 65 | 144 | 0 | 0 | 0 | 0 | 0 | 0 | 118 | 0 | 28 | 0 | 568 | 2205 |
| 4:30 PM | 0 | 122 | 87 | 0 | 57 | 133 | 0 | 0 | 0 | 0 | 0 | 0 | 114 | 0 | 19 | 0 | 532 | 2207 |
| 4:45 PM | 0 | 112 | 98 | 0 | 61 | 128 | 0 | 0 | 0 | 0 | 0 | 0 | 106 | 0 | 21 | 0 | 526 | 2154 |
| 5:00 PM | 0 | 138 | 89 | 0 | 69 | 141 | 0 | 0 | 0 | 0 | 0 | 0 | 114 | 0 | 31 | 0 | 582 | 2208 |
| 5:15 PM | 0 | 108 | 94 | 0 | 54 | 151 | 0 | 0 | 0 | 0 | 0 | 0 | 88 | 0 | 28 | 0 | 523 | 2163 |
| 5:30 PM | 0 | 89 | 77 | 0 | 49 | 116 | 0 | 0 | 0 | 0 | 0 | 0 | 79 | 0 | 29 | 0 | 439 | 2070 |
| 5:45 PM | 0 | 67 | 52 | 0 | 29 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 82 | 0 | 21 | 0 | 358 | 1902 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 552 | 356 | 0 | 276 | 564 | 0 | 0 | 0 | 0 | 0 | 0 | 456 | 0 | 124 | 0 |  | 28 |
| Heavy Trucks Buses | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |
| Pedestrians |  | 0 |  |  |  | 4 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |

Comments:






Peak-Hour: 3:45 PM -- 4:45 PM
Peak 15-Min: 3:45 PM -- 4:00 PM

Quality Counts
DATA THAT DRNES COMMUNITES


| 15-Min Count Period Beginning At | 37122 - NE Douglas Ave (Northbound) |  |  |  | 37122 - NE Douglas Ave (Southbound) |  |  |  | NE Diamond Lake Blvd (Eastbound) |  |  |  | NE Diamond Lake Blvd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 2:00 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 0 | 0 | 0 | 69 | 0 | 0 | 138 |  |
| 2:15 PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 88 | 2 | 0 | 0 | 83 | 0 | 0 | 175 |  |
| 2:30 PM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 108 | 3 | 0 | 3 | 86 | 0 | 0 | 203 |  |
| 2:45 PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 133 | 3 | 0 | 0 | 99 | 0 | 0 | 237 | 753 |
| 3:00 PM | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 109 | 1 | 0 | 1 | 139 | 0 | 0 | 253 | 868 |
| 3:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 111 | 1 | 0 | 1 | 122 | 0 | 0 | 236 | 929 |
| 3:30 PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 113 | 1 | 0 | 3 | 129 | 0 | 0 | 248 | 974 |
| 3:45 PM | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 118 | 3 | 0 | 2 | 155 | 0 | 0 | 282 | 1019 |
| 4:00 PM | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 123 | 2 | 0 | 0 | 115 | 0 | 0 | 244 | 1010 |
| 4:15 PM | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 112 | 0 | 0 | 2 | 162 | 0 | 0 | 279 | 1053 |
| 4:30 PM | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 121 | 0 | 0 | 2 | 131 | 0 | 0 | 257 | 1062 |
| 4:45 PM | 1 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 133 | 1 | 0 | 0 | 105 | 0 | 0 | 244 | 1024 |
| 5:00 PM | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 133 | 0 | 0 | 0 | 112 | 0 | 0 | 247 | 1027 |
| 5:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 145 | 0 | 0 | 1 | 88 | 0 | 0 | 235 | 983 |
| 5:30 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 125 | 0 | 0 | 1 | 62 | 0 | 0 | 189 | 915 |
| 5:45 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 80 | 0 | 0 | 2 | 72 | 0 | 0 | 155 | 826 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 4 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 472 | 12 | 0 | 8 | 620 | 0 | 0 |  | 28 |
| Heavy Trucks Buses | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:


Peak-Hour: 2:00 PM -- 3:00 PM
Peak 15-Min: 2:30 PM -- 2:45 PM


| 15-Min Count Period Beginning At | 37123 - NE Rifle Range Rd (Northbound) |  |  |  | 37123 - NE Rifle Range Rd (Southbound) |  |  |  | NE Douglas Ave (Eastbound) |  |  |  | NE Douglas Ave (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 2:00 PM | 0 | 0 | 0 | 0 | 9 | 0 | 20 | 0 | 8 | 7 | 0 | 0 | 0 | 9 | 5 | 0 | 58 |  |
| 2:15 PM | 0 | 0 | 0 | 0 | 3 | 0 | 18 | 0 | 9 | 13 | 0 | 0 | 0 | 8 | 5 | 0 | 56 |  |
| 2:30 PM | 0 | 0 | 0 | 0 | 7 | 0 | 15 | 0 | 30 | 15 | 0 | 0 | 0 | 10 | 13 | 0 | 90 |  |
| 2:45 PM | 0 | 0 | 0 | 0 | 7 | 0 | 4 | 0 | 18 | 7 | 0 | 0 | 0 | 9 | 9 | 0 | 54 | 258 |
| 3:00 PM | 0 | 0 | 0 | 0 | 8 | 0 | 12 | 0 | 5 | 5 | 0 | 0 | 0 | 7 | 8 | 0 | 45 | 245 |
| 3:15 PM | 0 | 0 | 0 | 0 | 2 | 0 | 15 | 0 | 6 | 5 | 0 | 0 | 0 | 4 | 4 | 0 | 36 | 225 |
| 3:30 PM | 0 | 0 | 0 | 0 | 3 | 0 | 9 | 0 | 15 | 8 | 0 | 0 | 0 | 6 | 7 | 0 | 48 | 183 |
| 3:45 PM | 0 | 0 | 0 | 0 | 3 | 0 | 18 | 0 | 9 | 12 | 0 | 0 | 0 | 6 | 8 | 0 | 56 | 185 |
| 4:00 PM | 0 | 0 | 0 | 0 | 4 | 0 | 10 | 0 | 15 | 4 | 0 | 0 | 0 | 4 | 4 | 0 | 41 | 181 |
| 4:15 PM | 0 | 0 | 0 | 0 | 8 | 0 | 7 | 0 | 17 | 6 | 0 | 0 | 0 | 3 | 3 | 0 | 44 | 189 |
| 4:30 PM | 0 | 0 | 0 | 0 | 9 | 0 | 12 | 1 | 14 | 4 | 0 | 0 | 0 | 4 | 8 | 0 | 52 | 193 |
| 4:45 PM | 0 | 0 | 0 | 0 | 10 | 0 | 13 | 1 | 13 | 11 | 0 | 0 | 0 | 5 | 2 | 0 | 55 | 192 |
| 5:00 PM | 0 | 0 | 0 | 0 | 9 | 0 | 15 | 0 | 14 | 8 | 0 | 0 | 0 | 6 | 7 | 0 | 59 | 210 |
| 5:15 PM | 0 | 0 | 0 | 0 | 11 | 0 | 14 | 0 | 11 | 4 | 0 | 1 | 0 | 8 | 4 | 0 | 53 | 219 |
| 5:30 PM | 0 | 0 | 0 | 0 | 5 | 0 | 13 | 0 | 8 | 5 | 0 | 0 | 0 | 6 | 3 | 0 | 40 | 207 |
| 5:45 PM | 0 | 0 | 0 | 0 | 5 | 0 | 11 | 0 | 5 | 5 | 0 | 0 | 0 | 7 | 4 | 0 | 37 | 189 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 0 | 0 | 0 | 28 | 0 | 60 | 0 | 120 | 60 | 0 | 0 | 0 | 40 | 52 | 0 |  | 0 |
| Heavy Trucks Buses | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  | 0 |

Comments:



Peak-Hour: 4:30 PM -- 5:30 PM
Peak 15-Min: 5:00 PM -- 5:15 PM

DATA THAT DRNES COMMUNITES


| 15-Min Count Period Beginning At | 37127 - NE Stephens St (Northbound) |  |  |  | 37127 - NE Stephens St (Southbound) |  |  |  | NE Winchester St (Eastbound) |  |  |  | NE Winchester St (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 2:00 PM | 0 | 133 | 3 | 0 | 109 | 215 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 121 | 0 | 581 |  |
| 2:15 PM | 0 | 165 | 1 | 0 | 86 | 191 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 73 | 0 | 516 |  |
| 2:30 PM | 0 | 184 | 1 | 0 | 112 | 188 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 91 | 0 | 576 |  |
| 2:45 PM | 0 | 162 | 0 | 0 | 101 | 172 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 110 | 0 | 545 | 2218 |
| 3:00 PM | 0 | 169 | 1 | 0 | 105 | 205 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 110 | 0 | 590 | 2227 |
| 3:15 PM | 0 | 177 | 2 | 0 | 78 | 195 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 122 | 0 | 574 | 2285 |
| 3:30 PM | 0 | 152 | 0 | 0 | 124 | 215 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 114 | 0 | 605 | 2314 |
| 3:45 PM | 0 | 165 | 1 | 0 | 96 | 160 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 123 | 0 | 545 | 2314 |
| 4:00 PM | 0 | 172 | 2 | 0 | 98 | 212 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 106 | 0 | 590 | 2314 |
| 4:15 PM | 0 | 160 | 3 | 0 | 99 | 188 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 101 | 0 | 551 | 2291 |
| 4:30 PM | 0 | 159 | 2 | 0 | 109 | 185 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 107 | 0 | 562 | 2248 |
| 4:45 PM | 0 | 157 | 0 | 0 | 107 | 210 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 101 | 0 | 575 | 2278 |
| 5:00 PM | 0 | 162 | 0 | 0 | 128 | 243 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 118 | 0 | 651 | 2339 |
| 5:15 PM | 0 | 174 | 0 | 0 | 120 | 210 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 103 | 0 | 607 | 2395 |
| 5:30 PM | 0 | 160 | 3 | 0 | 117 | 184 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 90 | 0 | 554 | 2387 |
| 5:45 PM | 0 | 115 | 1 | 0 | 99 | 131 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 103 | 0 | 449 | 2261 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 0 | 648 | 0 | 0 | 512 | 972 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 472 | 0 |  | 04 |
| Heavy Trucks Buses | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |

Comments:

Peak-Hour: 4:15 PM -- 5:15 PM
Peak 15-Min: 5:00 PM -- 5:15 PM
Quality Counts
DATA THAT DRNES COMMUNITES


| 15-Min Count Period Beginning At | 999110127 - NE Fowler St (Northbound) |  |  |  | 999110127 - NE Fowler St (Southbound) |  |  |  | NE Diamond Lake Blvd(Eastbound) |  |  |  | NE Diamond Lake Blvd (Westbound) |  |  |  | Total | Hourly Totals |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |
| 2:00 PM | 4 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 176 | 11 | 0 | 8 | 161 | 0 | 0 | 370 |  |
| 2:15 PM | 4 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 121 | 8 | 0 | 14 | 154 | 0 | 0 | 314 |  |
| 2:30 PM | 7 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 203 | 8 | 0 | 11 | 166 | 0 | 0 | 407 |  |
| 2:45 PM | 7 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 201 | 7 | 0 | 9 | 165 | 0 | 0 | 404 | 1495 |
| 3:00 PM | 6 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 203 | 2 | 0 | 14 | 191 | 0 | 0 | 425 | 1550 |
| 3:15 PM | 6 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 171 | 8 | 0 | 9 | 224 | 0 | 0 | 423 | 1659 |
| 3:30 PM | 4 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 184 | 6 | 0 | 13 | 210 | 0 | 0 | 430 | 1682 |
| 3:45 PM | 2 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 180 | 9 | 0 | 21 | 229 | 0 | 0 | 457 | 1735 |
| 4:00 PM | 6 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 208 | 6 | 0 | 18 | 231 | 0 | 0 | 488 | 1798 |
| 4:15 PM | 1 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 225 | 5 | 0 | 23 | 197 | 0 | 0 | 468 | 1843 |
| 4:30 PM | 7 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 187 | 10 | 0 | 11 | 235 | 0 | 0 | 464 | 1877 |
| 4:45 PM | 5 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 242 | 9 | 0 | 10 | 215 | 0 | 0 | 491 | 1911 |
| 5:00 PM | 9 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 240 | 12 | 0 | 10 | 195 | 0 | 0 | 493 | 1916 |
| 5:15 PM | 1 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 221 | 8 | 0 | 9 | 161 | 0 | 0 | 421 | 1869 |
| 5:30 PM | 2 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 195 | 12 | 0 | 9 | 156 | 0 | 0 | 384 | 1789 |
| 5:45 PM | 1 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 185 | 3 | 0 | 7 | 153 | 0 | 0 | 357 | 1655 |
| Peak 15-Min Flowrates | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  | Total |  |
|  | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U |  |  |  |
| All Vehicles | 36 | 0 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 960 | 48 | 0 | 40 | 780 | 0 | 0 |  | 72 |
| Heavy Trucks Buses | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |
| Pedestrians |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  | 0 |  |  |  |  |
| Bicycles Scooters | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  |

Comments:


## Appendix C Existing Traffic Conditions Worksheet

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [DiamondLake_Winchester (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.1.200

## New Site <br> Site Category: (None) <br> Yield (Two-Way)

Vehicle Movement Performance

| Mov ID |  | Mov Class | DemandArrival <br> Flows Flows[ Total HV [ [ Total HV ]veh/h \% veh/h \% |  |  |  | Deg. Satn <br> v/c | Aver. <br> Delay <br> sec | Level of Service |  | $\begin{aligned} & \text { ack of } \\ & \text { Dist ] } \\ & \text { ft } \end{aligned}$ | Prop. Que | $\begin{aligned} & \text { Eff. } \\ & \text { Stop } \\ & \text { Rate } \end{aligned}$ | Aver. No. of Cycles | Aver. Speed <br> mph |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Stephens St |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | All MCs | 841 | 1.0 | 841 | 1.0 | 0.233 | 0.9 | LOS A | 0.3 | 8.7 | 0.04 | 0.03 | 0.04 | 39.1 |
| 18 | R2 | All MCs | 9 | 0.0 | 9 | 0.0 | 0.233 | 120.4 | LOS F | 0.3 | 8.7 | 0.07 | 0.06 | 0.07 | 36.6 |
| Appr |  |  | 851 | 1.0 | 851 | 1.0 | 0.233 | 1.2 | NA | 0.3 | 8.7 | 0.04 | 0.03 | 0.04 | 39.1 |
| East: Winchester St |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | All MCs | 1 | 0.0 | 1 | 0.0 | 0.824 | 3288.9 | LOS F | 19.7 | 493.0 | 1.00 | 1.59 | 3.04 | 23.8 |
| 16 | R2 | All MCs | 539 | 0.0 | 539 | 0.0 | 0.824 | 28.2 | LOS D | 19.7 | 493.0 | 1.00 | 1.59 | 3.04 | 23.9 |
| Approach |  |  | 540 | 0.0 | 540 | 0.0 | 0.824 | 29.0 | LOS D | 19.7 | 493.0 | 1.00 | 1.59 | 3.04 | 23.9 |
| North: Stephens St |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | All MCs | 537 | 0.0 | 537 | 0.0 | 0.670 | 16.3 | LOS C | 7.7 | 192.8 | 0.81 | 1.17 | 2.05 | 27.5 |
| 4 | T1 | All MCs | 1032 | 1.0 | 1032 | 1.0 | 0.274 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 39.9 |
| Approach |  |  | 1569 | 0.7 | 1569 | 0.7 | 0.670 | 5.6 | NA | 7.7 | 192.8 | 0.28 | 0.40 | 0.70 | 34.6 |
| All Vehicles |  |  | 2960 | 0.6 | 2960 | 0.6 | 0.824 | 10.0 | NA | 19.7 | 493.0 | 0.34 | 0.51 | 0.94 | 32.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Minor Road Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Two-Way Sign Control Capacity Model: SIDRA Standard (HCM).
Delay Model: HCM Delay Formula (Stopline Delay: Geometric Delay is not included).
Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.
Gap-Acceptance Capacity Formula: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

[^7]Queues
2: SE Stephens St \& NE Diamond Lake Blvd

|  | 7 | $4$ | $\uparrow$ | 7 |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Group Flow (vph) | 523 | 114 | 606 | 425 | 288 | 661 |
| v/c Ratio | 0.45 | 0.08 | 0.70 | 0.41 | 0.75 | 0.41 |
| Control Delay | 16.3 | 0.1 | 35.9 | 2.4 | 28.4 | 15.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 16.3 | 0.1 | 35.9 | 2.4 | 28.4 | 15.7 |
| Queue Length 50th ( t ) | 52 | 0 | 175 | 10 | 104 | 128 |
| Queue Length 95th ( t ) | 98 | 0 | 214 | 42 | 136 | 134 |
| Internal Link Dist (ft) | 453 |  | 312 |  |  | 334 |
| Turn Bay Length (ft) |  |  |  | 120 | 200 |  |
| Base Capacity (vph) | 1153 | 1430 | 985 | 1056 | 516 | 2013 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.45 | 0.08 | 0.62 | 0.40 | 0.56 | 0.33 |

[^8]
c Critical Lane Group


HCM 6th Signalized Intersection Capacity Analysis
2: SE Stephens St \& NE Diamond Lake Blvd

| Lanes in Grp | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grp Vol (v), veh/h | 0 | 0 | 0 | 523 | 288 | 0 | 0 | 0 |
| Grp Sat Flow (s), veh/h/ln | 0 | 0 | 0 | 1503 | 1628 | 0 | 0 | 0 |
| Q Serve Time (g_s), s | 0.0 | 0.0 | 0.0 | 11.7 | 12.2 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear Time (g_c), s | 0.0 | 0.0 | 0.0 | 11.7 | 12.2 | 0.0 | 0.0 | 0.0 |
| Perm LT Sat Flow (s_l), veh/h/ln | 0 | 0 | 0 | 1503 | 543 | 0 | 0 | 0 |
| Shared LT Sat Flow (s_sh), veh/h/ln | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Perm LT Eff Green (g_p), s | 0.0 | 0.0 | 0.0 | 0.0 | 23.2 | 0.0 | 0.0 | 0.0 |
| Perm LT Serve Time (g_u), s | 0.0 | 0.0 | 0.0 | 0.0 | 7.0 | 0.0 | 0.0 | 0.0 |
| Perm LT Q Serve Time (g_ps), s | 0.0 | 0.0 | 0.0 | 0.0 | 7.0 | 0.0 | 0.0 | 0.0 |
| Time to First Blk (g_f), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 23.2 | 0.0 | 0.0 |
| Serve Time pre Blk (g_fs), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop LT Inside Lane (P_L) | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 |
| Lane Grp Cap (c), veh/h | 0 | 0 | 0 | 1245 | 370 | 0 | 0 | 0 |
| V/C Ratio (X) | 0.00 | 0.00 | 0.00 | 0.42 | 0.78 | 0.00 | 0.00 | 0.00 |
| Avail Cap (c_a), veh/h | 0 | 0 | 0 | 1245 | 529 | 0 | 0 | 0 |
| Upstream Filter (I) | 0.00 | 0.00 | 0.00 | 0.92 | 1.00 | 0.00 | 0.00 | 0.00 |
| Uniform Delay (d1), s/veh | 0.0 | 0.0 | 0.0 | 19.7 | 23.1 | 0.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 1.0 | 3.8 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 20.7 | 26.9 | 0.0 | 0.0 | 0.0 |
| $1 \mathrm{st-Term} \mathrm{Q}$ (Q1), veh/ln | 0.0 | 0.0 | 0.0 | 3.9 | 4.4 | 0.0 | 0.0 | 0.0 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.0 | 0.0 | 0.2 | 0.4 | 0.0 | 0.0 | 0.0 |
| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q Factor ( f_B\%) | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| \%ile Back of Q ( $50 \%$ ), veh/ln | 0.0 | 0.0 | 0.0 | 4.1 | 4.8 | 0.0 | 0.0 | 0.0 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.00 | 0.00 | 0.25 | 0.62 | 0.00 | 0.00 | 0.00 |
| Initial $Q(Q b)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


| Middle Lane Group Data |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Mvmt | 0 | 2 | 0 | 4 | 0 | 6 | 0 | 0 |
| Lane Assignment |  | $T$ |  |  |  | $T$ |  |  |
| Lanes in Grp | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 |
| Grp Vol (v), veh/h | 0 | 661 | 0 | 0 | 0 | 606 | 0 | 0 |
| Grp Sat Flow (s), veh/h/ln | 0.0 | 1250 | 0 | 0 | 0 | 1650 | 0 | 0 |
| Q Serve Time (g_s), s | 0.0 | 12.8 | 0.0 | 0.0 | 0.0 | 16.2 | 0.0 | 0.0 |
| Cycle Q Clear Time (g_c), s | 0 | 1526 | 0 | 0 | 0.0 | 16.2 | 0.0 | 0.0 |
| Lane Grp Cap (c), veh/h | 0.00 | 0.43 | 0.00 | 0.00 | 0.00 | 805 | 0 | 0 |
| V/C Ratio (X) | 0 | 2018 | 0 | 0 | 0 | 969 | 0.00 | 0.00 |
| Avail Cap (c_a), veh/h | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0 | 0 |
| Upstream Filter (I) | 0.0 | 17.2 | 0.0 | 0.0 | 0.0 | 33.2 | 0.0 | 0.0 |
| Uniform Delay (d1), s/veh | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 3.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay (d3), s/veh | 0.0 | 17.5 | 0.0 | 0.0 | 0.0 | 36.5 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 4.6 | 0.0 | 0.0 | 0.0 | 6.3 | 0.0 | 0.0 |
| 1st-Term Q (Q1), veh/l/n | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |
| 2nd-Term Q (Q2), veh/ln |  |  |  |  |  |  |  |  |

HCM 6th Signalized Intersection Capacity Analysis
2: SE Stephens St \& NE Diamond Lake Blvd

| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| \%ile Back of Q Factor (f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| \%ile Back of Q (550\%), veh/ln | 0.0 | 4.6 | 0.0 | 0.0 | 0.0 | 6.6 | 0.0 | 0.0 |
| \%ili Storage Ratio (RQ\%) | 0.00 | 0.32 | 0.00 | 0.00 | 0.00 | 0.46 | 0.00 | 0.00 |
| Initial Q (Qb), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Right Lane Group Data

| Assigned Mvmt | 0 | 12 | 0 | 14 | 0 | 16 | 0 | 0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Assignment |  |  |  | R |  | R |  |  |  |
| Lanes in Grp | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 |  |
| Grp Vol (v), veh/h | 0 | 0 | 0 | 0 | 0 | 425 | 0 | 0 |  |
| Grp Sat Flow (s), veh/h/ln | 0 | 0 | 0 | 1437 | 0 | 1385 | 0 | 0 |  |
| Q Serve Time (g_s), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.4 | 0.0 | 0.0 |  |
| Cycle Q Clear Time (g_c), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 14.4 | 0.0 | 0.0 |  |
| Prot RT Sat Flow (s_R), veh/h/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1390.5 | 0.0 | 0.0 |  |
| Prot RT Eff Green (g_R), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 39.4 | 0.0 | 0.0 |  |
| Prop RT Outside Lane (P_R) | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |
| Lane Grp Cap (c), veh/h | 0 | 0 | 0 | 595 | 0 | 914 | 0 | 0 |  |
| VIC Ratio (X) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.46 | 0.00 | 0.00 |  |
| Avail Cap (c_a), veh/h | 0 | 0 | 0 | 595 | 0 | 983 | 0 | 0 |  |
| Upstream Filter (I) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |
| Uniform Delay (d1), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.0 | 0.0 | 0.0 |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 |  |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Control Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 8.6 | 0.0 | 0.0 |  |
| 1st-Term Q (Q1), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 9.9 | 0.0 | 0.0 |  |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |  |
| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| \%ile Back of Q Factor ( f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |  |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.0 | 0.0 | 0.0 |  |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.22 | 0.00 | 0.00 |  |
| Initial $Q(Q b)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Final (Residual) $\mathrm{Q}(\mathrm{Qe})$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

## Intersection Summary

HCM 6th Ctrl Delay 22.3
HCM 6th LOS
C

## Notes

* HCM 6th Edition computational engine requires equal clearance times for the phases crossing the barrier.

User approved changes to right turn type.
Unsignalized Delay for [WBR] is excluded from calculations of the approach delay and intersection delay.

Queues
3: NE Winchester St/SE Jackson St \& NE Diamond Lake Blvd

|  | $\rangle$ | $\rightarrow$ | 7 | 7 | 4 | 4 | 4 | $\uparrow$ | 7 | , | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Group Flow (vph) | 46 | 590 | 47 | 25 | 531 | 418 | 10 | 81 | 25 | 406 | 169 |
| v/c Ratio | 0.35 | 0.41 | 0.06 | 0.22 | 0.40 | 0.36 | 0.10 | 0.48 | 0.09 | 0.90 | 0.27 |
| Control Delay | 41.4 | 26.7 | 0.5 | 45.8 | 23.3 | 2.3 | 44.0 | 49.1 | 0.6 | 57.6 | 14.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.4 | 26.7 | 0.5 | 45.8 | 23.3 | 2.3 | 44.0 | 49.1 | 0.6 | 57.6 | 14.6 |
| Queue Length 50th ( t ) | 28 | 157 | 0 | 15 | 132 | 10 | 6 | 47 | 0 | 225 | 41 |
| Queue Length 95th (ft) | m55 | 237 | m2 | 40 | 200 | 49 | 22 | 90 | 0 | \#396 | 100 |
| Internal Link Dist (ft) |  | 453 |  |  | 292 |  |  | 86 |  |  | 62 |
| Turn Bay Length (ft) | 100 |  | 60 | 85 |  | 50 | 80 |  | 80 | 155 |  |
| Base Capacity (vph) | 181 | 1450 | 761 | 133 | 1324 | 1160 | 190 | 331 | 408 | 478 | 672 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.25 | 0.41 | 0.06 | 0.19 | 0.40 | 0.36 | 0.05 | 0.24 | 0.06 | 0.85 | 0.25 |

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
m Volume for 95 th percentile queue is metered by upstream signal.

HCM Signalized Intersection Capacity Analysis
3: NE Winchester St/SE Jackson St \& NE Diamond Lake Blvd
08/09/2023

c Critical Lane Group

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Through Movement Data

| Assigned Mvmt | 2 | 4 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: |
| Mvmt Sat Flow, veh/h | 3143 | 858 | 3092 | 1750 |
| Right-Turn Movement Data |  |  |  |  |
| Assigned Mvmt | 12 | 14 | 16 | 18 |
| Mvmt Sat Flow, veh/h | 1480 | 753 | 1480 | 1466 |

## Left Lane Group Data

| Assigned Mvmt | 1 | 0 | 3 | 0 | 5 | 0 | 7 | 0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Assignment | L (Prot) | L (Prot) | L (Prot) |  | $\mathrm{L}($ Prot $)$ |  |  |  |

HCM 6th Signalized Intersection Capacity Analysis
3: NE Winchester St/SE Jackson St \& NE Diamond Lake Blvd

| Lanes in Grp | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grp Vol (v), veh/h | 25 | 0 | 10 | 0 | 46 | 0 | 406 | 0 |
| Grp Sat Flow (s), veh/h/ln | 1654 | 0 | 1654 | 0 | 1654 | 0 | 1667 | 0 |
| Q Serve Time (g_s), s | 1.4 | 0.0 | 0.6 | 0.0 | 2.6 | 0.0 | 22.6 | 0.0 |
| Cycle Q Clear Time (g_c), s | 1.4 | 0.0 | 0.6 | 0.0 | 2.6 | 0.0 | 22.6 | 0.0 |
| Perm LT Sat Flow (s_l), veh/h/ln | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Shared LT Sat Flow (s_sh), veh/h/ln | 0 | 0 | 0 | 0 | 0 | O | 0 | 0 |
| Perm LT Eff Green (g_p), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Perm LT Serve Time (g_u), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Perm LT Q Serve Time (g_ps), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Time to First Blk (g_f), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Serve Time pre Blk (g_fs), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop LT Inside Lane (P_L) | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Lane Grp Cap (c), veh/h | 42 | 0 | 20 | 0 | 61 | 0 | 436 | 0 |
| V/C Ratio (X) | 0.59 | 0.00 | 0.50 | 0.00 | 0.75 | 0.00 | 0.93 | 0.00 |
| Avail Cap (c_a), veh/h | 131 | 0 | 191 | 0 | 183 | 0 | 474 | 0 |
| Upstream Filter (I) | 1.00 | 0.00 | 1.00 | 0.00 | 0.82 | 0.00 | 1.00 | 0.00 |
| Uniform Delay (d1), s/veh | 45.8 | 0.0 | 46.6 | 0.0 | 45.3 | 0.0 | 34.2 | 0.0 |
| Incr Delay (d2), s/veh | 9.6 | 0.0 | 13.3 | 0.0 | 10.7 | 0.0 | 23.9 | 0.0 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 55.4 | 0.0 | 59.9 | 0.0 | 56.0 | 0.0 | 58.1 | 0.0 |
| 1st-Term Q (Q1), veh/ln | 0.6 | 0.0 | 0.2 | 0.0 | 1.1 | 0.0 | 8.8 | 0.0 |
| 2nd-Term Q (Q2), veh/ln | 0.1 | 0.0 | 0.1 | 0.0 | 0.2 | 0.0 | 2.9 | 0.0 |
| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q Factor ( f B\%) | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| \%ile Back of Q (50\%), veh/ln | 0.7 | 0.0 | 0.3 | 0.0 | 1.2 | 0.0 | 11.7 | 0.0 |
| \%ile Storage Ratio (RQ\%) | 0.20 | 0.00 | 0.10 | 0.00 | 0.31 | 0.00 | 1.89 | 0.00 |
| Initial $Q(Q b)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

## Middle Lane Group Data

| Assigned Mvmt | 0 | 2 | 0 | 4 | 0 | 6 | 0 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Assignment |  | $T$ |  |  |  | $T$ |  | $T$ |
| Lanes in Grp | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 1 |
| Grp Vol (v), veh/h | 0 | 590 | 0 | 0 | 0 | 531 | 0 | 81 |
| Grp Sat Flow (s), veh/h/ln | 0 | 1572 | 0 | 0 | 0 | 1546 | 0 | 1750 |
| Q Serve Time (g_s), s | 0.0 | 11.9 | 0.0 | 0.0 | 0.0 | 10.9 | 0.0 | 4.3 |
| Cycle Q Clear Time (g_c), s | 0.0 | 11.9 | 0.0 | 0.0 | 0.0 | 10.9 | 0.0 | 4.3 |
| Lane Grp Cap (c), veh/h | 0 | 1435 | 0 | 0 | 0 | 1375 | 0 | 136 |
| V/C Ratio (X) | 0.00 | 0.41 | 0.00 | 0.00 | 0.00 | 0.39 | 0.00 | 0.60 |
| Avail Cap (c_a), veh/h | 0 | 1435 | 0 | 0 | 0 | 1375 | 0 | 332 |
| Upstream Filter (I) | 0.00 | 0.82 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d1), s/veh | 0.0 | 17.3 | 0.0 | 0.0 | 0.0 | 17.7 | 0.0 | 42.4 |
| Incr Delay (d2), s/veh | 0.0 | 0.7 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 3.1 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 18.0 | 0.0 | 0.0 | 0.0 | 18.5 | 0.0 | 45.5 |
| 1st-Term Q (Q1), veh/ln | 0.0 | 4.1 | 0.0 | 0.0 | 0.0 | 3.7 | 0.0 | 1.8 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 |

HCM 6th Signalized Intersection Capacity Analysis
3: NE Winchester St/SE Jackson St \& NE Diamond Lake Blvd

| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| \%ile Back of Q Factor (f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 4.2 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | 1.9 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.26 | 0.00 | 0.00 | 0.00 | 0.36 | 0.00 | 0.44 |
| Initial Q (Qb), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

## Right Lane Group Data



Intersection Summary

HCM 6th Ctrl Delay 26.0

HCM 6th LOS
C

## Notes

User approved pedestrian interval to be less than phase max green.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 个 |  |  |  |  |  |
| Traffic Vol, veh/h | 974 | 34 | 70 | 992 | 21 | 68 |
| Future Vol, veh/h | 974 | 34 | 70 | 992 | 21 | 68 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 0 | - | 50 | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1004 | 35 | 72 | 1023 | 22 | 70 |





Queues
6: NE Rifle Range Rd \& NE Diamond Lake Blvd

|  | $\rangle$ | $\rightarrow$ | 7 |  | 4 | T |  | $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 46 | 871 | 13 | 769 | 94 | 29 | 3 | 33 |
| v/c Ratio | 0.11 | 0.43 | 0.04 | 0.35 | 0.39 | 0.10 | 0.01 | 0.11 |
| Control Delay | 6.1 | 6.3 | 5.4 | 5.9 | 23.1 | 9.5 | 16.7 | 9.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 6.1 | 6.3 | 5.4 | 5.9 | 23.1 | 9.5 | 16.7 | 9.2 |
| Queue Length 50th (ft) | 5 | 57 | 1 | 50 | 20 | 1 | 1 | 1 |
| Queue Length 95th (ft) | 19 | 114 | 8 | 97 | 63 | 18 | 6 | 19 |
| Internal Link Dist (ft) |  | 695 |  | 509 |  | 305 |  | 334 |
| Turn Bay Length (ft) |  |  |  |  | 225 |  |  |  |
| Base Capacity (vph) | 569 | 2840 | 518 | 3062 | 702 | 838 | 718 | 826 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.08 | 0.31 | 0.03 | 0.25 | 0.13 | 0.03 | 0.00 | 0.04 |

[^9]HCM Signalized Intersection Capacity Analysis
6: NE Rifle Range Rd \& NE Diamond Lake Blvd
08/09/2023


Analysis Period (min)
15
C Critical Lane Group

HCM 6th Signalized Intersection Capacity Analysis
6: NE Rifle Range Rd \& NE Diamond Lake Blvd

|  | $\rangle$ | $\rightarrow$ |  | 7 | 4 | 4 | 4 | $\dagger$ | p |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个t |  | ${ }^{7}$ | 中 ${ }^{\text {d }}$ |  | 7 | F |  | ${ }^{7}$ | F |  |
| Traffic Volume (veh/h) | 43 | 698 | 120 | 12 | 714 | 8 | 88 | 3 | 24 | 3 | 3 | 28 |
| Future Volume (veh/h) | 43 | 698 | 120 | 12 | 714 | 8 | 88 | 3 | 24 | 3 | 3 | 28 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial Q, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj (A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Lanes Open During Work Zone |  |  |  |  |  |  |  |  |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 1723 | 1668 | 1723 | 1750 | 1750 | 1750 | 1723 | 1750 | 1736 | 1750 | 1695 | 1723 |
| Adj Flow Rate, veh/h | 46 | 743 | 128 | 13 | 760 | 9 | 94 | 3 | 26 | 3 | 3 | 30 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh, \% | 2 | 6 | 2 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 4 | 2 |
| Opposing Right Turn Influence | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |
| Cap, veh/h | 492 | 1519 | 262 | 444 | 1892 | 22 | 352 | 22 | 187 | 359 | 18 | 184 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Prop Arrive On Green | 0.56 | 0.56 | 0.56 | 0.56 | 0.56 | 0.56 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| Unsig. Movement Delay |  |  |  |  |  |  |  |  |  |  |  |  |
| Ln Grp Delay, s/veh | 6.7 | 5.9 | 5.9 | 7.2 | 5.3 | 5.2 | 16.2 | 0.0 | 14.7 | 14.8 | 0.0 | 14.8 |
| Ln Grp LOS | A | A | A | A | A | A | B | A | B | B | A | B |
| Approach Vol, veh/h |  | 917 |  |  | 782 |  |  | 123 |  |  | 36 |  |
| Approach Delay, s/veh |  | 5.9 |  |  | 5.3 |  |  | 15.8 |  |  | 14.8 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |


| Timer: | 1 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Through Movement Data |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :---: |
| Assigned Mvmt | 2 | 4 | 6 | 8 |  |
| Mvmt Sat Flow, veh/h | 2701 | 132 | 3365 | 155 |  |
| Right-Turn Movement Data |  |  |  |  |  |
| Assigned Mrmt | 12 | 14 | 16 | 18 |  |
| Mvmt Sat Flow, veh/h | 465 | 1320 | 40 | 1346 |  |


| Left Lane Group Data | 0 | 5 | 0 | 7 | 0 | 1 | 0 | 3 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Assigned Mvmt |  | L |  | L |  | L |  | L |
| Lane Assignment |  |  |  |  |  |  |  |  |

HCM 6th Signalized Intersection Capacity Analysis
6: NE Rifle Range Rd \& NE Diamond Lake Blvd

| Lanes in Grp | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grp Vol (v), veh/h | 0 | 46 | 0 | 3 | 0 | 13 | 0 | 94 |
| Grp Sat Flow (s), veh/h/ln | 0 | 699 | 0 | 1397 | 0 | 645 | 0 | 1371 |
| Q Serve Time (g_s), s | 0.0 | 1.5 | 0.0 | 0.1 | 0.0 | 0.5 | 0.0 | 2.5 |
| Cycle Q Clear Time (g_c), s | 0.0 | 6.4 | 0.0 | 0.7 | 0.0 | 6.8 | 0.0 | 3.2 |
| Perm LT Sat Flow (s_l), veh/h/ln | 0 | 699 | 0 | 1397 | 0 | 645 | 0 | 1371 |
| Shared LT Sat Flow (s_sh), veh/h/ln | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Perm LT Eff Green (g_p), s | 0.0 | 21.5 | 0.0 | 5.3 | 0.0 | 21.5 | 0.0 | 5.3 |
| Perm LT Serve Time (g_u), s | 0.0 | 16.6 | 0.0 | 4.7 | 0.0 | 15.1 | 0.0 | 4.6 |
| Perm LT Q Serve Time (g_ps), s | 0.0 | 1.5 | 0.0 | 0.1 | 0.0 | 0.5 | 0.0 | 2.5 |
| Time to First Blk (g_f), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Serve Time pre Blk (g_fs), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop LT Inside Lane (P_L) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap (c), veh/h | 0 | 492 | 0 | 359 | 0 | 444 | 0 | 352 |
| V/C Ratio (X) | 0.00 | 0.09 | 0.00 | 0.01 | 0.00 | 0.03 | 0.00 | 0.27 |
| Avail Cap (c_a), veh/h | 0 | 922 | 0 | 1079 | 0 | 841 | 0 | 1058 |
| Upstream Filter (I) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d1), s/veh | 0.0 | 6.5 | 0.0 | 14.7 | 0.0 | 7.1 | 0.0 | 15.9 |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.3 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 6.7 | 0.0 | 14.8 | 0.0 | 7.2 | 0.0 | 16.2 |
| 1st-Term Q (Q1), veh/In | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q Factor (f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.07 |
| Initial Q (Qb), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Middle Lane Group Data |  |  |  |  |  |  |  |  |
| Assigned Mvmt | 0 | 2 | 0 | 4 | 0 | 6 | 0 | 8 |
| Lane Assignment |  | T |  |  |  | T |  |  |
| Lanes in Grp | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 |
| Grp Vol (v), veh/h | 0 | 436 | 0 | 0 | 0 | 375 | 0 | 0 |
| Grp Sat Flow (s), veh/h/ln | 0 | 1585 | 0 | 0 | 0 | 1663 | 0 | 0 |
| Q Serve Time (g_s), s | 0.0 | 6.3 | 0.0 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 |
| Cycle Q Clear Time (g_c), s | 0.0 | 6.3 | 0.0 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 |
| Lane Grp Cap (c), veh/h | 0 | 891 | 0 | 0 | 0 | 935 | 0 | 0 |
| V/C Ratio (X) | 0.00 | 0.49 | 0.00 | 0.00 | 0.00 | 0.40 | 0.00 | 0.00 |
| Avail Cap (c_a), veh/h | 0 | 1867 | 0 | 0 | 0 | 1958 | 0 | 0 |
| Upstream Filter (I) | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d1), s/veh | 0.0 | 5.0 | 0.0 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.8 | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 5.9 | 0.0 | 0.0 | 0.0 | 5.3 | 0.0 | 0.0 |
| 1st-Term Q (Q1), veh/In | 0.0 | 0.9 | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |

HCM 6th Signalized Intersection Capacity Analysis
6: NE Rifle Range Rd \& NE Diamond Lake Blvd

| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| \%ole Back of Q Factor (f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| \%ole Back of Q (50\%), veh/ln | 0.0 | 1.1 | 0.0 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.04 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 |
| Initial Q (Qb), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Right Lane Group Data

| Assigned Mvmt | 0 | 12 | 0 | 14 | 0 | 16 | 0 | 18 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Assignment |  | T+R |  | T+R |  | T+R |  | T+R |
| Lanes in Grp | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| Grp Vol (v), veh/h | 0 | 435 | 0 | 33 | 0 | 394 | 0 | 29 |
| Grp Sat Flow (s), veh/h/ln | 0 | 1582 | 0 | 1452 | 0 | 1743 | 0 | 1502 |
| Q Serve Time (g_s), s | 0.0 | 6.3 | 0.0 | 0.8 | 0.0 | 4.9 | 0.0 | 0.6 |
| Cycle Q Clear Time (g_c), s | 0.0 | 6.3 | 0.0 | 0.8 | 0.0 | 4.9 | 0.0 | 0.6 |
| Prot RT Sat Flow (s_R), veh/h/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prot RT Eff Green (g_R), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop RT Outside Lane (P_R) | 0.00 | 0.29 | 0.00 | 0.91 | 0.00 | 0.02 | 0.00 | 0.90 |
| Lane Grp Cap (c), veh/h | 0 | 890 | 0 | 202 | 0 | 980 | 0 | 209 |
| VIC Ratio (X) | 0.00 | 0.49 | 0.00 | 0.16 | 0.00 | 0.40 | 0.00 | 0.14 |
| Avail Cap (c_a), veh/h | 0 | 1863 | 0 | 950 | 0 | 2053 | 0 | 983 |
| Upstream Filter (I) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d1), s/veh | 0.0 | 5.0 | 0.0 | 14.5 | 0.0 | 4.7 | 0.0 | 14.4 |
| Incr Delay (d2), s/veh | 0.0 | 0.8 | 0.0 | 0.3 | 0.0 | 0.5 | 0.0 | 0.2 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 5.9 | 0.0 | 14.8 | 0.0 | 5.2 | 0.0 | 14.7 |
| 1st-Term Q (Q1), veh/ln | 0.0 | 0.9 | 0.0 | 0.2 | 0.0 | 0.5 | 0.0 | 0.2 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |
| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q Factor (f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 1.1 | 0.0 | 0.2 | 0.0 | 0.7 | 0.0 | 0.2 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.04 | 0.00 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 |
| Initial $Q(Q b)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


| Intersection Summary |  |
| :--- | :--- |
| HCM 6th Ctrl Delay | 6.5 |

HCM 6th LOS A

## Notes

User approved pedestrian interval to be less than phase max green.

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 㻢 |  | ${ }^{*}$ | 44 | M |  |
| Traffic Vol, veh/h | 553 | 3 | 5 | 580 | 5 | 12 |
| Future Vol, veh/h | 553 | 3 | 5 | 580 | 5 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 75 | - | 0 | - |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 1 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 4 | 0 | 11 | 4 | 0 | 7 |
| Mvmt Flow | 601 | 3 | 5 | 630 | 5 | 13 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 604 | 0 | 928 | 302 |
| Stage 1 | - | - | - | - | 603 | - |
| Stage 2 | - | - | - | - | 325 | - |
| Critical Hdwy | - | - | 4.32 | - | 6.8 | 7.04 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.8 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.8 | - |
| Follow-up Hdwy | - | - | 2.31 | - | 3.5 | 3.37 |
| Pot Cap-1 Maneuver | - | - | 911 | - | 271 | 679 |
| Stage 1 | - | - | - | - | 515 | - |
| Stage 2 | - | - | - | - | 711 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 911 | - | 270 | 679 |
| Mov Cap-2 Maneuver | - | - | - | - | 390 | - |
| Stage 1 | - | - | - | - | 515 | - |
| Stage 2 | - | - | - | - | 707 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.1 |  | 11.7 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 557 | - | - | 911 | - |
| HCM Lane V/C Ratio |  | 0.033 | - |  | 0.006 | - |
| HCM Control Delay (s) |  | 11.7 | - | - | 9 | - |
| HCM Lane LOS |  | B | - | - | A | - |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |

Queues
8: SE Stephens St \& SE Douglas Ave

|  | $\rangle$ | $\rightarrow$ | 7 |  | 4 | $\dagger$ | , | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Group Flow (vph) | 85 | 43 | 135 | 124 | 8 | 1158 | 82 | 1257 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.19 | 0.06 | 0.34 | 0.24 | 0.05 | 0.85 | 0.44 | 0.53 |
| Control Delay | 24.4 | 17.9 | 37.8 | 20.6 | 24.1 | 39.1 | 22.7 | 20.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.4 | 17.9 | 37.8 | 20.6 | 24.1 | 39.1 | 22.7 | 20.2 |
| Queue Length 50th ( ft ) | 42 | 15 | 85 | 41 | 4 | 435 | 31 | 231 |
| Queue Length 95th (t) | 72 | 36 | 139 | 85 | 15 | 502 | 54 | 247 |
| Internal Link Dist (ft) |  | 389 |  | 479 |  | 92 |  | 142 |
| Turn Bay Length (ft) |  |  |  |  | 100 |  | 150 |  |
| Base Capacity (vph) | 485 | 679 | 394 | 527 | 146 | 1364 | 268 | 2379 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.18 | 0.06 | 0.34 | 0.24 | 0.05 | 0.85 | 0.31 | 0.53 |

[^10]HCM Signalized Intersection Capacity Analysis
8: SE Stephens St \& SE Douglas Ave
08/09/2023

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

HCM 6th Signalized Intersection Capacity Analysis
8: SE Stephens St \& SE Douglas Ave

|  | 4 | $\rightarrow$ |  | $\dagger$ |  | 4 | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\square}$ |  | \% | $\uparrow$ |  | \% | 性 |  | ${ }^{7}$ | 楽 |  |
| Traffic Volume (veh/h) | 71 | 26 | 10 | 113 | 43 | 61 | 7 | 877 | 96 | 69 | 1028 | 28 |
| Future Volume (veh/h) | 71 | 26 | 10 | 113 | 43 | 61 | 7 | 877 | 96 | 69 | 1028 | 28 |
| Number | 3 | 8 | 18 | 7 | 4 | 14 | 1 | 6 | 16 | 5 | 2 | 12 |
| Initial Q, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj (A_pbT) | 1.00 |  | 0.99 | 0.99 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 0.98 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Lanes Open During Work Zone |  |  |  |  |  |  |  |  |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1682 | 1750 | 1750 | 1682 | 1736 |
| Adj Flow Rate, veh/h | 85 | 31 | 12 | 135 | 51 | 73 | 8 | 1044 | 114 | 82 | 1224 | 33 |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| Percent Heavy Veh, \% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 1 |
| Opposing Right Turn Influence | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |
| Cap, veh/h | 290 | 292 | 113 | 367 | 158 | 226 | 313 | 1984 | 216 | 309 | 3137 | 85 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Prop Arrive On Green | 0.00 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 | 0.68 | 0.68 | 0.68 | 0.00 | 0.68 | 0.68 |
| Unsig. Movement Delay |  |  |  |  |  |  |  |  |  |  |  |  |
| Ln Grp Delay, s/veh | 44.5 | 0.0 | 36.6 | 43.9 | 0.0 | 40.4 | 11.9 | 11.5 | 11.4 | 18.0 | 9.0 | 9.4 |
| Ln Grp LOS | D | A | D | D | A | D | B | B | B | B | A | A |
| Approach Vol, veh/h |  | 128 |  |  | 259 |  |  | 1166 |  |  | 1339 |  |
| Approach Delay, s/veh |  | 41.9 |  |  | 42.2 |  |  | 11.5 |  |  | 9.7 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | A |  |


| Timer: | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Leff-Turn Movement Data

| Assigned Mvmt | 3 | 7 | 5 | 1 |
| :--- | ---: | ---: | ---: | ---: |
| Mvmt Sat Flow, veh/h | 1667 | 1377 | 1667 | 449 |

Through Movement Data

| Assigned Mvmt | 2 | 4 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: |
| Mvmt Sat Flow, veh/h | 4593 | 648 | 2905 | 1199 |
| Right-Turn Movement Data |  |  |  |  |
| Assigned Mvmt | 12 | 14 | 16 | 18 |
| Mvmt Sat Flow, veh/h | 124 | 928 | 317 | 464 |


| Leff Lane Group Data |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Assigned Mvmt | 0 | 0 | 3 | 7 | 5 | 1 | 0 | 0 |
| Lane Assignment |  | $L(P r / P m)$ | $\amalg(P r / P m)$ | L |  |  |  |  |

HCM 6th Signalized Intersection Capacity Analysis
8: SE Stephens St \& SE Douglas Ave

| Lanes in Grp | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grp Vol (v), veh/h | 0 | 0 | 85 | 135 | 82 | 8 | 0 | 0 |
| Grp Sat Flow (s), veh/h/ln | 0 | 0 | 1667 | 1377 | 1667 | 449 | 0 | 0 |
| Q Serve Time (g_s), s | 0.0 | 0.0 | 0.1 | 10.4 | 0.1 | 1.0 | 0.0 | 0.0 |
| Cycle Q Clear Time (g_c), s | 0.0 | 0.0 | 0.1 | 12.8 | 0.1 | 15.1 | 0.0 | 0.0 |
| Perm LT Sat Flow (s_l), veh/h/ln | 0 | 0 | 1282 | 1377 | 493 | 449 | 0 | 0 |
| Shared LT Sat Flow (s_sh), veh/h/ln | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Perm LT Eff Green (g_p), s | 0.0 | 0.0 | 32.0 | 30.0 | 84.0 | 84.0 | 0.0 | 0.0 |
| Perm LT Serve Time (g_u), s | 0.0 | 0.0 | 22.1 | 27.5 | 62.1 | 69.8 | 0.0 | 0.0 |
| Perm LT Q Serve Time (g_ps), s | 0.0 | 0.0 | 7.0 | 10.4 | 11.7 | 1.0 | 0.0 | 0.0 |
| Time to First Blk (g_f), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Serve Time pre Blk (g_fs), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop LT Inside Lane (P_L) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Lane Grp Cap (c), veh/h | 0 | 0 | 290 | 367 | 309 | 313 | 0 | 0 |
| V/C Ratio (X) | 0.00 | 0.00 | 0.29 | 0.37 | 0.27 | 0.03 | 0.00 | 0.00 |
| Avail Cap (c_a), veh/h | 0 | 0 | 492 | 367 | 511 | 313 | 0 | 0 |
| Upstream Filter (I) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d1), s/veh | 0.0 | 0.0 | 44.1 | 41.1 | 17.5 | 11.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.4 | 2.8 | 0.5 | 0.2 | 0.0 | 0.0 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 0.0 | 44.5 | 43.9 | 18.0 | 11.9 | 0.0 | 0.0 |
| 1st-Term Q (Q1), veh/ln | 0.0 | 0.0 | 2.3 | 3.6 | 1.3 | 0.1 | 0.0 | 0.0 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 |
| 3rd-Term Q (Q3), veh/In | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q Factor (f_B\%) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 0.0 | 2.3 | 3.9 | 1.3 | 0.1 | 0.0 | 0.0 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.00 | 0.14 | 0.21 | 0.22 | 0.03 | 0.00 | 0.00 |
| Initial $Q(Q b)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Middle Lane Group Data |  |  |  |  |  |  |  |  |
| Assigned Mvmt | 0 | 2 | 0 | 4 | 0 | 6 | 0 | 8 |
| Lane Assignment |  | T |  |  |  | T |  |  |
| Lanes in Grp | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 |
| Grp Vol (v), veh/h | 0 | 816 | 0 | 0 | 0 | 574 | 0 | 0 |
| Grp Sat Flow (s), veh/h/ln | 0 | 1530 | 0 | 0 | 0 | 1598 | 0 | 0 |
| Q Serve Time (g_s), s | 0.0 | 14.2 | 0.0 | 0.0 | 0.0 | 21.9 | 0.0 | 0.0 |
| Cycle Q Clear Time (g_c), s | 0.0 | 14.2 | 0.0 | 0.0 | 0.0 | 21.9 | 0.0 | 0.0 |
| Lane Grp Cap (c), veh/h | 0 | 2090 | 0 | 0 | 0 | 1091 | 0 | 0 |
| V/C Ratio (X) | 0.00 | 0.39 | 0.00 | 0.00 | 0.00 | 0.53 | 0.00 | 0.00 |
| Avail Cap (c_a), veh/h | 0 | 2090 | 0 | 0 | 0 | 1091 | 0 | 0 |
| Upstream Filter (I) | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d1), s/veh | 0.0 | 8.4 | 0.0 | 0.0 | 0.0 | 9.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 1.8 | 0.0 | 0.0 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 9.0 | 0.0 | 0.0 | 0.0 | 11.5 | 0.0 | 0.0 |
| 1st-Term Q (Q1), veh/ln | 0.0 | 4.3 | 0.0 | 0.0 | 0.0 | 6.9 | 0.0 | 0.0 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 |

HCM 6th Signalized Intersection Capacity Analysis
8: SE Stephens St \& SE Douglas Ave

| 3rd-Term Q (Q3), veh/l/n | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| \%ile Back of Q Factor (f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 4.4 | 0.0 | 0.0 | 0.0 | 7.5 | 0.0 | 0.0 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.62 | 0.00 | 0.00 | 0.00 | 1.44 | 0.00 | 0.00 |
| Initial Q (Qb), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) Q (Qe), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Right Lane Group Data

| Assigned Mvmt | 0 | 12 | 0 | 14 | 0 | 16 | 0 | 18 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Assignment |  | T+R |  | T+R |  | T+R |  | T+R |
| Lanes in Grp | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 |
| Grp Vol (v), veh/h | 0 | 441 | 0 | 124 | 0 | 584 | 0 | 43 |
| Grp Sat Flow (s), veh/h/ln | 0 | 1656 | 0 | 1576 | 0 | 1624 | 0 | 1663 |
| Q Serve Time (g_s), s | 0.0 | 14.2 | 0.0 | 7.9 | 0.0 | 21.9 | 0.0 | 2.5 |
| Cycle Q Clear Time (g_c), s | 0.0 | 14.2 | 0.0 | 7.9 | 0.0 | 21.9 | 0.0 | 2.5 |
| Prot RT Sat Flow (s_R), veh/h/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prot RT Eff Green (g_R), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop RT Outside Lane (P_R) | 0.00 | 0.07 | 0.00 | 0.59 | 0.00 | 0.20 | 0.00 | 0.28 |
| Lane Grp Cap (c), veh/h | 0 | 1131 | 0 | 384 | 0 | 1109 | 0 | 406 |
| V/C Ratio (X) | 0.00 | 0.39 | 0.00 | 0.32 | 0.00 | 0.53 | 0.00 | 0.11 |
| Avail Cap (c_a), veh/h | 0 | 1131 | 0 | 384 | 0 | 1109 | 0 | 406 |
| Upstream Filter (I) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d1), s/veh | 0.0 | 8.4 | 0.0 | 38.2 | 0.0 | 9.7 | 0.0 | 36.1 |
| Incr Delay (d2), s/veh | 0.0 | 1.0 | 0.0 | 2.2 | 0.0 | 1.8 | 0.0 | 0.5 |
| Initial Q Delay (d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Control Delay (d), s/veh | 0.0 | 9.4 | 0.0 | 40.4 | 0.0 | 11.4 | 0.0 | 36.6 |
| 1st-Term Q (Q1), veh/ln | 0.0 | 4.6 | 0.0 | 3.1 | 0.0 | 7.0 | 0.0 | 1.0 |
| 2nd-Term Q (Q2), veh/ln | 0.0 | 0.3 | 0.0 | 0.2 | 0.0 | 0.6 | 0.0 | 0.1 |
| 3rd-Term Q (Q3), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q Factor ( f_B\%) | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| \%ile Back of Q (50\%), veh/ln | 0.0 | 5.0 | 0.0 | 3.4 | 0.0 | 7.6 | 0.0 | 1.1 |
| \%ile Storage Ratio (RQ\%) | 0.00 | 0.70 | 0.00 | 0.18 | 0.00 | 1.46 | 0.00 | 0.07 |
| Initial $Q(Q b)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Final (Residual) $Q(Q e)$, veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Delay (ds), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Q (Qs), veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Sat Cap (cs), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q Clear Time (tc), h | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Intersection Summary
HCM 6th Ctrl Delay 14.7

HCM 6th LOS
B

## Notes

User approved pedestrian interval to be less than phase max green.

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | * $\uparrow$ |  |  |  |  |  | * $\uparrow$ |  |
| Traffic Vol, veh/h | 40 | 197 | 32 | 26 | 162 | 103 | 0 | 0 | 0 | 69 | 71 | 24 |
| Future Vol, veh/h | 40 | 197 | 32 | 26 | 162 | 103 | 0 | 0 | 0 | 69 | 71 | 24 |
| Conflicting Peds, \#/hr | 6 | 0 | 6 | 6 | 0 | 6 | 7 | 0 | 7 | 7 | 0 | 7 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | 25 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | 108222 | 6688 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 45 | 224 | 36 | 30 | 184 | 117 | 0 | 0 | 0 | 78 | 81 | 27 |






| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 358 | 0 | - | 0 | 559 | 308 |
| Stage 1 | - | - | - | - | 308 | - |
| Stage 2 | - | - | - | - | 251 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1201 | - | - | - | 490 | 732 |
| Stage 1 | - | - | - | - | 745 | - |
| Stage 2 | - | - | - | - | 791 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1201 | - | - | - | 485 | 732 |
| Mov Cap-2 Maneuver | - | - | - | - | 485 | - |
| Stage 1 | - | - | - | - | 737 | - |
| Stage 2 | - | - | - | - | 791 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.4 |  | 0 |  | 13.7 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1201 | - | - | - | 517 |
| HCM Lane V/C Ratio |  | 0.01 | - | - | - | 0.203 |
| HCM Control Delay (s) |  | 8 | 0 | - | - | 13.7 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.8 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 5.6 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\mathbf{b}$ |  |  | $\mathbf{-}$ | $\mathbf{1}$ | $\mathbf{7}$ |
| Traffic Vol, veh/h | 68 | 97 | 55 | 53 | 102 | 56 |
| Future Vol, veh/h | 68 | 97 | 55 | 53 | 102 | 56 |
| Conflicting Peds, \#/hr | 0 | 1 | 1 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 50 | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 65 | 65 | 65 | 65 | 65 | 65 |
| Heavy Vehicles, \% | 0 | 0 | 1 | 1 | 0 | 2 |
| Mvmt Flow | 105 | 149 | 85 | 82 | 157 | 86 |






[^0]:    ${ }^{1}$ The designations and recommendations as part of the OR 138E Design Concept Plan, if applicable, will take precedence over the City's Transportation System Plan.
    ${ }^{2}$ Level of traffic stress categories are ratings and are not performance measures.

[^1]:    ${ }^{3}$ Analysis Procedure Manual (APM Version 2), Chapter 4-Safety, Oregon Department of Transportation
    ${ }^{4}$ https://www.oregon.gov/odot/engineering/pages/spis-reports-on-state.aspx

[^2]:    ${ }^{5}$ Oregon Transportation Safety Data Explorer (OTSDE) (arcgis.com)

[^3]:    ${ }^{7}$ https://www.oregon.gov/odot/engineering/pages/spis-reports-on-state.aspx

[^4]:    Note:

    * Indicates one of the crashes involved a bicyclist

[^5]:    ${ }^{8}$ Analysis Procedure Manual (APM Version 2), Chapter 4-Safety, Oregon Department of Transportation

[^6]:    ${ }^{9}$ Five-Year Comparison of State Highway Crash Rates
    ${ }^{10}$ Critical Rate Calculator
    ${ }^{11}$ Analysis Procedures Manual Chapters 1-4 (oregon.gov)

[^7]:    SIDRA INTERSECTION 9.1 | Copyright © 2000-2022 Akcelik and Associates Pty Ltd | sidrasolutions.com
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    Project: H:\23\23021 - Transportation and Land Use Planningl032 - Diamond Lake Boulevard Corridor Studylanalysis\sidral23021_032_Sidra.sip9

[^8]:    Intersection Summary

[^9]:    Intersection Summary

[^10]:    Intersection Summary

